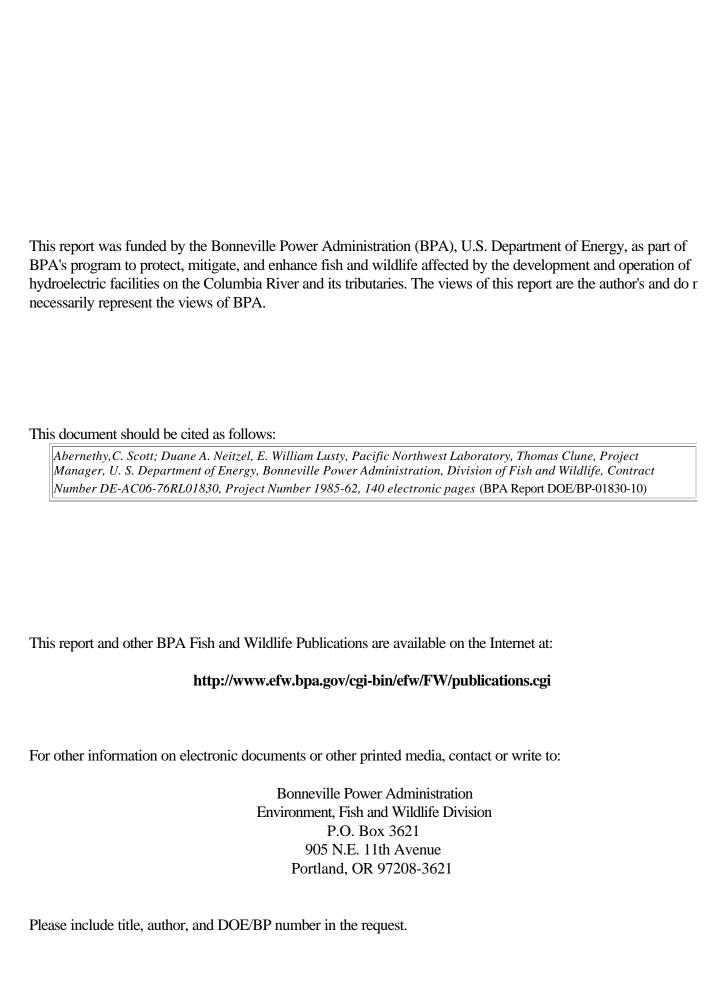
September 1989

VELOCITY MEASUREMENTS AT THREE FISH SCREENING FACILITIES IN THE YAKIMA RIVER BASIN, WASHINGTON ANNUAL REPORT SUMMER 1989

Annual Report 1989







VELOCITY MEASUREMENTS AT THREE FISH SCREENING FACILITIES

IN THE YAKIMA RIVER BASIN, WASHINGTON

ANNUAL REPORT

SUMMER 1989

bу

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PREFACE

The Bonneville Power Administration and the U.S. Bureau of Reclamation are funding the construction and evaluation of fish passage and protection facilities at irrigation and hydroelectric diversions in the Yakima River Basin, Washington State. This construction implements Sections 903(d) and 803(b) of the Northwest Power Planning Council's 1984 and 1987 Columbia River Basin Fish and Wildlife Program (a) The program provides offsite enhancement to compensate for fish and wildlife losses caused by hydroelectric development throughout the Columbia River Basin, and addresses natural propagation of salmon to help mitigate the impact of irrigation in the Yakima River Basin.

The Wapato. Chandler, and Easton screens are three of the juvenile screening facilities. This report evaluates the flow characteristics of the screening facilities. Studies consisted of velocity measurements taken in front of the rotary drum screens and within the fish bypass systems during peak flows. Measurements of approach velocity and sweep velocity were emphasized in these studies: however, vertical velocity was also measured. Results indicate that velocity patterns within the screening facilities often differ from design specifications, but are generally conducive to effective fish bypass.

⁽a) NPPC (Northwest Power Planning Council). 1984. Columbia River Basin Fish and Wildlife Program Northwest Power Planning Council, Portland, Oregon.

NPPC (Northwest Power Planning Council). 1987. Columbia River as in Fish and Wildlife Program Northwest Power Planning Council, Portland, Oregon.

ACKNOWLEDGEMENTS

The involvement and cooperation of many people during these studies are greatly appreciated. Thoms J. Clune of the Bonneville Power Administration was the Project Manager. Robert Pearce of the National Marine Fisheries Service, NMFS. and Ken Bates of the Washington Department of Fisheries reviewed the plans for measuring velocities. Chuck Keller of the Bureau of Reclamation and his operations and maintenance staffs provided critical support and assistance during site preparation and data collection. Alvin L. Jensen , NMFS. provided the instrumentation used in our studies. The manuscript was reviewed by Regina E. Lundgren and Wallace H. Walters.

ABSTRACT

The Pacific Northwest Laboratory (PNL)^(a) measured the velocity conditions at three fish screening facilities in the Yakima River Basin: Wapato. Chandler, and Easton Screens. The measurement objectives were different at the three screens. At Wapato. approach and sweep velocities were measured to evaluate the effect of rearing pens in the screen forebay. A complete survey was preformed at the Chandler Screens. At Easton, velocity was measured behind the screens to provide information for the installation of porosity boards to balance flow through the screens.

Salmon-rearing pens used at the Wapato Canal had a minimal effect on the magnitude of approach and sweep velocities at the face of the drum screens, although the pens caused increased turbulence and variability in water velocities. The net pens did not appear to affect flows through the three fish bypasses.

Approach velocities at the Chandler Screens ranged from 0.1 fps at the upper end of the screening facility to >0.5 fps at the downstream end of the facility. Sweep velocity was generally <1.0 fps in the screen forebay, especially under the curvature of the drum screens. Low sweep velocities and elevated approach velocities under the curvature of the drum screens result in velocity conditions that do not meet the design criteria standards. Flow through each of the three fish bypasses was X2.0 fps. Sweep velocity in the separation chamber was <1.0 fps at 0.8 of the depth. Approach velocity at the face of traveling screens in the separation chamber was <0.5 fps. Water velocities in the fish return met design criteria.

Approach velocities at the Easton Screens varied from 0.1 fps to >0.6 fps from the upstream to the downstream end of the screening facility. Inbalanced flows throughout the screen array may be partially attributable to water flow around a bend in the canal upstream of the screen forebay that results in high sweeping velocity along the outer wall of the screen forebay.

⁽a) The Pacific Northwest Laboratory is operated by the Battelle Memorial Institute for the U.S. Department of Energy under Contract DE-AC06-76RL0 1830.

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INTRODUCTION

The Pacific Northwest Electric Power Planning and Conservation Act (Public Law 96-501) was passed to enable preparation and implementation of a regional Conservation and Electric Power Plan. The Northwest Power Planning Council administers the plan, and is charged with developing a program to protect and enhance fish and wildlife populations and to mitigate adverse effects from development, operation, and management of hydroelectric facilities.

The Yakima River Basin was selected as one site for enhancement of salmon (Oncorhynchus spp.). Under the Plan, the Bonneville Power Administration (BPA) and the U.S. Bureau of Reclamation (BR) are funding the construction of fish passage and protection facilities at 20 existing irrigation and hydroelectric diversions in the Yakima River Basin (Figure 1).

The improvement of fish screening facilities in irrigation canals is a major component in the overall fisheries enhancement program. Hydrologists and biologists from various agencies, including the National Marine Fisheries Service (NMFS). the Washington Department of Fisheries, and the Yakima Indian Nation (YIN) provided input for the design of the new facilities. The angled rotary drum screen design was chosen as the best alternative for fish screening in irrigation canals.

Pacific Northwest Laboratory (PNL) conducted fisheries evaluations at six of the new fish screening facilities from 1985 through 1989 (Neitzel et al. 1985; 1987; 1988; 1990a; 1990b). The scope of the studies included the quantification of injury and mortality, predation, and passage effectiveness for emigrating salmonids: however, it did not include evaluating hydraulic characteristics within the screening facilities. The hydraulic conditions in front of the drum screens as well as within components of the fish guidance system (fish bypasses, separation chamber, and fish return slot) are critical in providing optimum conditions for safe fish bypass. The screens were designed to provide an approach velocity (perpendicular to the screens) of 0.5 feet per second (fps) or less to minimize impingement of fish and a sweep velocity (parallel to the screen face) of at least twice the magnitude of the approach velocity to guide fish into the bypass system (Easterbrooks 1984).

Inadequate sweep velocities, excessive approach velocities. or unequal discharges through the drum screens and fish bypass system have been observed at several of the screening facilities during our fisheries evaluations. These flow pattern anomalies can affect the overall efficiency of a facility. Velocity measurements were taken at six screen sites in 1988 (Abernethy et al. 1989) to monitor the actual velocity characteristics at selected facilities during normal operation, as defined by the operating criteria for each facility.

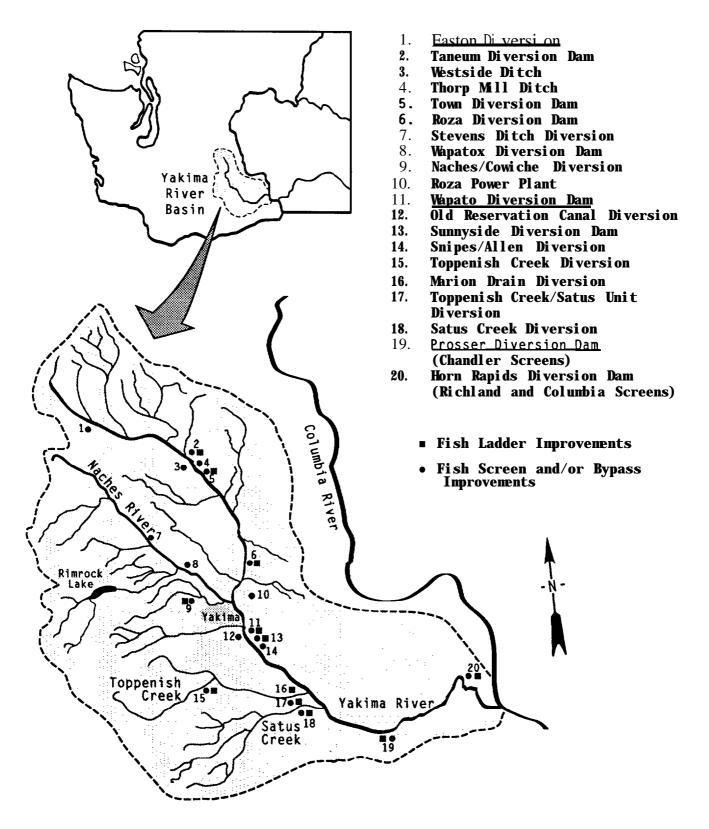


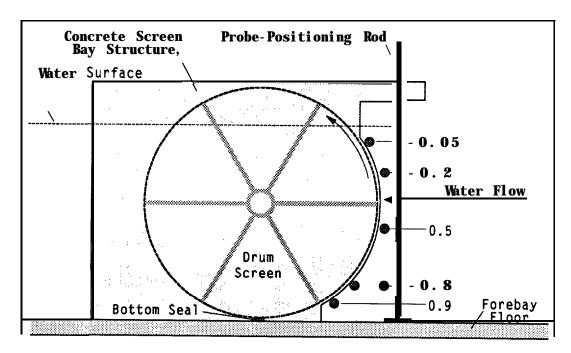
FIGURE I. Yakima River Basin Fish Screening Facilities and Other Fish Protection and Passage Facilities

This report describes additional velocity measurement studies conducted by PNL staff at the Wapato, Chandler, and Easton Screens in 1989. It describes the equipment and methods used to measure the hydraulic characteristics and the operating conditions at each facility during data collection, and summarizes the results and conclusions. The raw data are included in three appendixes (one for each site) to allow independent analysis of the data.

METHODS

Three monitoring protocols were used in our data collection based on the objectives of the measurements at each site. Measurements were taken at the Wapato Screens to evaluate the effect of the use of salmon-rearing pens in the canal forebay on flow parameters in front of the drum screens. Velocity readings for the X (approach velocity) and Y (sweep velocity) components were taken at 0.2 and 0.8 of the water depth in front of each drum screen and at the head of each fish bypass one day before and one hour after the net pens were removed from the Wapato Screens forebay. A complete survey, which included measurements at 0.05, 0.2, 0.5, 0.8, and 0.9 of the water depth in front of the drum screens and at 0.2 and 0.8 of the water depth in components of the fish bypass system was performed at the Wapato Screens in 1988 (Abernethy et al. 1989).

A complete survey was performed at the Chandler Screens. Velocity measurements were taken at 0.2 and 0.8 of the depth in front of each of the drum screens, in the fish bypasses, and in the separation chamber. Additional velocity measurements were taken at 0.05. 0.5, 0.8. and 0.9 of the depth in front of drum screens adjacent to each fish bypass (Figure 2). Velocity readings were taken to measure the X (approach velocity). Y (sweep velocity), and 2 (vertical velocity) components at all locations.



Probe Location

FIGURE. Measurement Depths and Probe Positioning Relative to the Front Face of Rotary Drum Screens in Complete Surveys

Velocity measurements were taken at 0.2 and 0.8 of the depth behind each of the drum screens at the Easton Screens to provide information for porosity board placement to balance flows through the screens. No flow measurements were taken in front of the drum screens or in the fish bypass system

EQUIPMENT

Electromagnetic water current meters were used to monitor water velocities. Each meter used a bidirectional probe (Figure 3). Probes were mounted in pairs at the Chandler Screens so that one measured the X and Y and the other measured the Y and Z velocity components at a given depth. The vertical velocity (Z) component was not measured at the Wapato and Easton Screens: therefore, only one probe was necessary at each measurement location. A smaller electromagnetic water current meter, which measures flow in one direction only, was also used at the Easton Screens to compare the data obtained from different instruments. Outputs were read visually from panel gauges.

The meter probes were securely fastened to a horizontal arm that extended from a movable sleeve secured to a vertical pole. The length of the horizontal arm and the position of the sleeve on the vertical pole were adjustable. The probe support assembly was positioned at least 18 in. downstream or outside of the sensors so that the vertical pole and horizontal bracket arm would not disrupt velocity readings at the probes.

PROBE POSITIONING

The position of the probes was adjusted for each of the measurement locations within the facility. Measurements were taken in or near the drum screens, fish bypasses. separation chamber, vertical traveling screens, and the fish return.

Cross Section of Probe

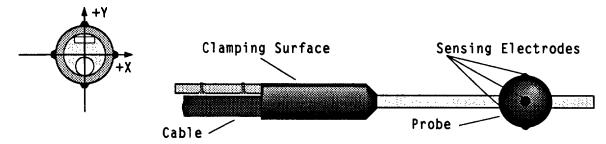
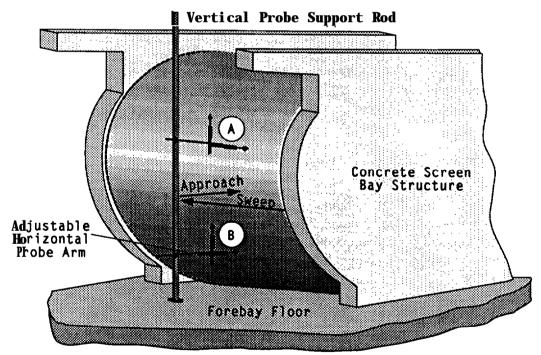


FIGURE. Bidirectional Electromagnetic Probes Used in Velocity Measurements

Measurements Near Drum Screens

For velocity measurements at the Wapato and Chandler screens, the vertical pole was positioned close to the perimeter in front of the screen; however. none of the components of the probe assembly were in contact with the The bottom of the pole rested on the forebay floor, and the screen face. top end of the pole was clamped to a fixed object, such as the gantry frame Measurements at 0.2, 0.5, and 0.8 of the depth were taken by or a girder. mounting the probes on a horizontal arm pointing upstream (Figure 4). and measurements near the screen face at 0.05, 0.8, and 0.9 of the depth were taken by mounting the probes on a horizontal arm pointed inward toward the face of the screen. The length of the horizontal arm required to position the probes close to the screen face was calculated based on screen diameter, water depth, and the position of the vertical pole relative to the perimeter of the screen. The set of probes was within $5 (\pm 1)$ in. of the screen face for the near-screen measurements. The drum screens are constructed at an angle to the canal flow: therefore, all measurements were taken with the probe orientation parallel and perpendicular to the screen All velocity measurements were taken at the face, not to the canal flow. centerline of the screen.



- Probes Pointed Upstream from Vertical Rod (Measurements at 0.2. 0.5. and 0.8 of the Depth)
- Probes Pointed Towards Screen Face (Measurements at 0.05. 0.8a. and 0.9 of the Depth:

FIGURF 4 Relationship of Probe Support Assembly to Probes During Velocity Measurements

For velocity measurements at the Easton Screens, the vertical pole was positioned at the centerline of each drum screen about 15 in. from the screen surface on the back side of the screen. The horizontal arm supporting the probe for the bidirectional flow meter was oriented upstream so that the X and Y components could be measured. The probe for the unidirectional flow meter was pointed directly at the screen face, then slowly rotated to achieve the highest stable reading on the panel gauge.

Measurements in the Fish Bypasses

Measurements were taken at 0.2 and 0.8 of the depth at the centerline of the 24-in.-wide fish bypasses at the Wapato and Chandler Screens. All bypasses had submerged ramps to guide fish and water up from the bottom of the screen structure and over an adjustable weir at the back of the ramp. The probes were positioned about 18 in. upstream of the ramp. This positioning generally placed the probes within the concrete structure of the bypass.

Measurements in the Separation Chamber

Measurements were taken at 0.2 and 0.8 of the depth in transects across the width of the separation chamber at the Chandler screens. Transects were made upstream of the vertical traveling screens and at the centerline of each traveling screen. The traveling screens were constructed perpendicular to the separation chamber flow, with the outer wall (distal to the traveling screens) angling toward the screens. The probes were positioned pointing upstream parallel to the traveling screens. Turbulent areas where bypass flows mix at the head of the separation chamber were not evaluated.

Measurements Near Vertical Traveling Screens

Measurements were taken at 0.2 and 0.8 of the depth at the face of the traveling screens. The probes were positioned parallel to the screen face at the centerline and in the upper and lower quadrants at the Chandler Screens. The measurements along the screen face and the transects across the separation chamber merged to form a "T" pattern of velocity measurements.

Measurements in the Fish Return

Velocity measurements were taken at 0.2 and 0.8 of the depth in the fish return at the Chandler Screens near the upstream end of the fish return slot. The vertical pole was positioned upstream of the submerged approach ramp, but within the concrete structure of the fish return slot.

DATA COLLECTION AND ANALYSIS

Ten sets of velocity measurements were recorded in a 3- to 5-min interval. Each set of readings provided a "snapshot" of all velocity measurements. Beginning and ending times were recorded for each series of data. Unusual operating or canal flow conditions were recorded as "Notes" on the data sheets. Analyses and comparisons were performed using the means of the data.

DESCRIPTION OF CONDITIONS AT FACH SITE

Our data were collected during the peak of the irrigation season under the existing operating conditions at each site. The Chandler Canal was not at full capacity because of the frequent flow adjustments required to meet in-river flow obligations during periods of low river flow. Surface elevation and/or forebay depth were determined from staff gages at each site. Actual daily canal flows were provided by the Bureau of Reclamation. Unusual flow or operating conditions were recorded at each site.

WAPATO_CANAL

The Wapato Screens (Figure 5) are located in the Wapato Canal on the right bank of the Yakima River at RM 106.7. The facility consists of 15 rotary drum screens (14 ft diameter, 24 ft long) and a fish bypass system that includes three fish bypasses (two intermediate and a terminal), a separation chamber with two bypass water recovery pumps located behind vertical traveling screens, and a fish return. The YIN uses the Wapato Screens forebay to house three pens for rearing fall chinook salmon (0.tshawytscha). The floating pens are attached to the outer wing wall opposite the screens near the second fish bypass (Figure 6).

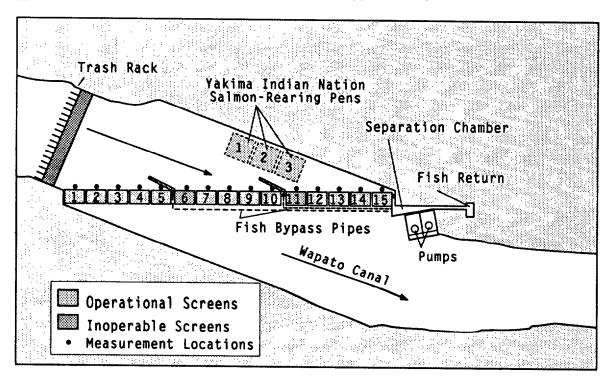


FIGURE. Locations of Facility Components and Rearing Pens at the Wapato Screens, Spring 1989

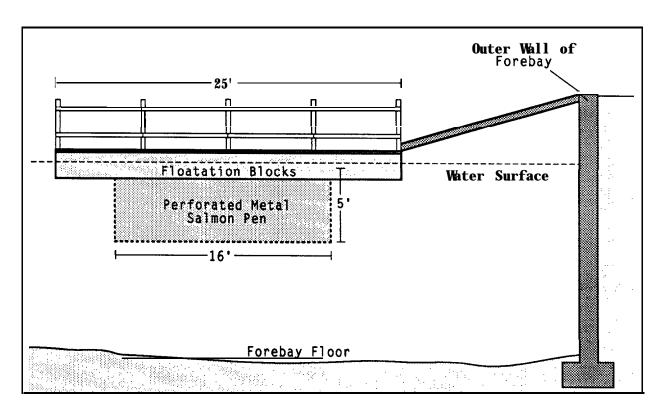


FIGURE. Pens Used by the Yakima Indian Nation to Rear Fall Chinook Salmon in the Wapato Screens Forebay

The forebay elevation is about 935 ft at the maximum canal flow of 1800 cubic feet per second (cfs). The first series of measurements was conducted at the Wapato Canal on June 1 and 2. 1989. Canal elevation was 934.9 ft, and the canal flow was 1830 cfs. Water depth in front of the screens was 140 in. Of the 168-in. drum screen diameter, 132 in. (79%) were submerged. We used the submerged screen depth as the basis for calculating probe positioning.

All operating conditions were normal (Appendix A) with the following exceptions:

- . The vertical traveling screens in the separation chamber were not in service.
- · Rotary drum screens 6 and 11 were not operational.
- .Three YIN salmon-rearing pens were in use in the screen forebay.

The second series of velocity measurements was completed on June 5 and 6. 1989, after the YIN salmon pens were removed from the canal forebay. The surface elevation in the canal was 934.85 ft, and the canal flow was 1850 cfs. All other operating conditions were the same as during the first series of measurements except that the three salmon net pens had been removed.

CHANDLER CANAL

The Chandler Screens (Figure 7) are located in the Chandler Canal on the right bank of the Yakima River. The head gates of the Chandler Canal withdraw water from the Yakima River at the Prosser Diversion Dam at RM 47.0 near Prosser. Washington. The facility consists of 24 rotary drum screens (13.5 ft diameter, 12 ft long) and a fish bypass system that includes three fish bypasses (two intermediate and a terminal), a separation chamber with four bypass water recovery pumps located behind vertical traveling screens, and a fish return. The forebay elevation is about 631 ft at the maximum canal flow of 1400 cfs.

A complete survey was conducted at the Chandler Screens on July 26 to 28, 1989. Canal elevation was 630.1 ft. and the canal flow was 1050 to 1100 cfs. Water depth in front of the screens was 112 in. Of the 162-in. drum screen diameter, 108 in. (67%) were submerged. We used the submerged screen depth as the basis for calculating probe positioning.

All operating conditions were normal Appendix A) with the following exceptions:

- . Screen 23 was inoperable and stoplogged shut.
- · Only two of the four bypass water return pumps were operating.

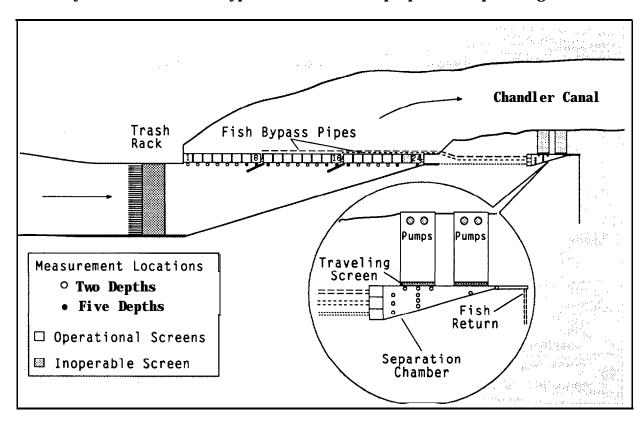


FIGURE. Locations of Facility Components at the Chandler Screens, Spring 1989

EASTON CANAL

The Easton Screens (Figure 8) are located in the Kittitas Main Canal on the right bank of the Yakima River at RM 202.5 near Easton, Washington. The facility consists of 18 rotary drum screens (15 ft diameter, 12 ft long) and a fish bypass system that includes two fish bypasses (intermediate and terminal), each with a flow of 20 cfs, and a fish return. The maximum canal flow is about 1200 cfs. Flow measurements were taken at the Easton Screens on June 14 and 15. 1989 with a canal flow of 1130 cfs. Water depth behind the screens was 139 in. All operating conditions were normal (Appendix A).

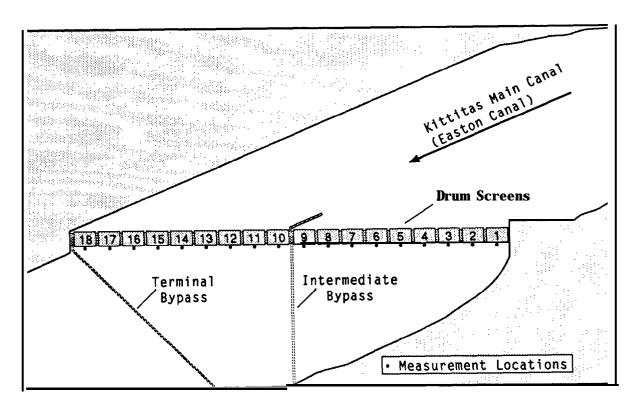


FIGURE. Probe Locations for Flow Velocity Measurements at the Easton Screens, Spring 1989

RFSUL TS

The objective of our velocity measurements differed at each of the three sites. Velocity measurements performed at the Wapato Screens evaluated flow conditions near the drum screens relative to the use of salmon-rearing pens in the screen forebay. A complete survey was performed at the Chandler Screens. Velocity measurements performed at the Easton Screens evaluated flow balance through the array of screens.

WAPATO SCREENS

Velocity measurements taken before and after the removal of three salmon-rearing pens from the Wapato Screens forebay indicated that although the pens had only a minimal effect on actual approach and sweep velocities at the face of the drum screens, the pens contributed to increased turbulence and instability of the water flow. Swirls and turbulence at the face of drum screens could result in intermittent increases in approach velocities. The net pens did not appear to affect flows through the three fish bypasses.

The magnitude of the approach velocity was not affected at 0.2 of the depth (Figure 9). 0.8 of the depth (Figure 10). or under the curvature of the screens at 0.8 of the depth (Figure 11). Variability of the approach velocity was greater at the two 0.8 readings when the pens were in use.

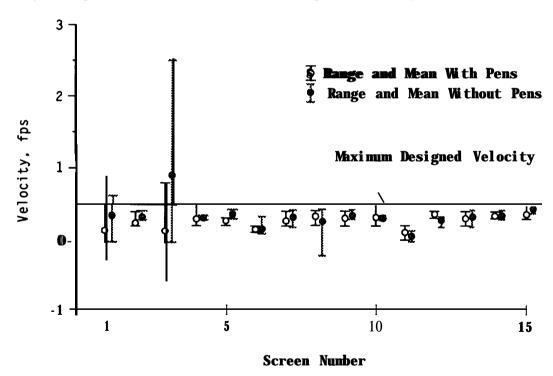


FIGURE 9. Approach Velocity at 0.2 of the Depth in Front of Drum Screens at the Wapato Canal, Spring 1989

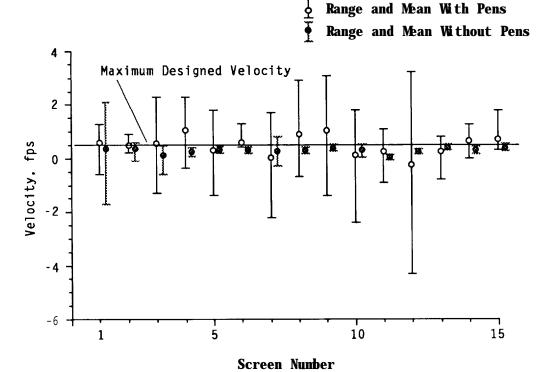


FIGURE 10. Approach Velocity at 0.8 of the Depth in Front of Drum Screens at the Wapato Canal, Spring 1989

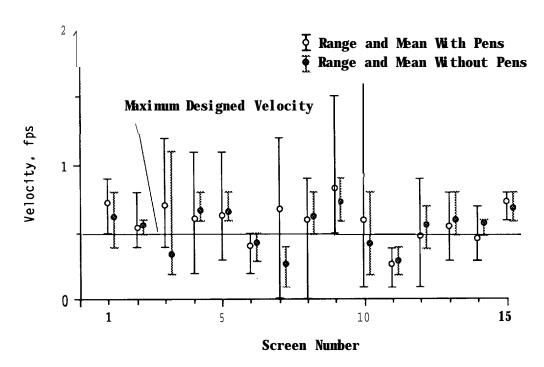


FIGURE 11. Approach Velocity at 0.8 of the Depth Under the Curvature of Drum Screens at the Wapato Canal, Spring 1989

Sweep velocity increased at 0.2 of the depth (Figure 12) and decreased at 0.8 of the depth (Figure 13) when the net pens were removed. Sweep velocity under the curvature of the drum screen at 0.8 of the depth was only slightly affected (Figure 14). Variation of the sweep velocity measurements was greater at all three of the measurement locations when the pens were in use.

Flow was balanced through the three fish bypasses both with and without the pens in the forebay. Velocity in each of the bypasses increased at 0.2 of the depth and decreased at 0.8 of the depth when the pens were removed (Table 1).

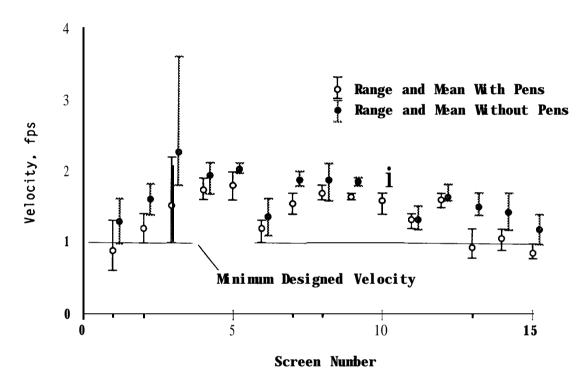


FIGURE 12. Sweep Velocity at 0.2 of the Depth in Front of Drum Screens at the Wapato Canal, Spring 1989

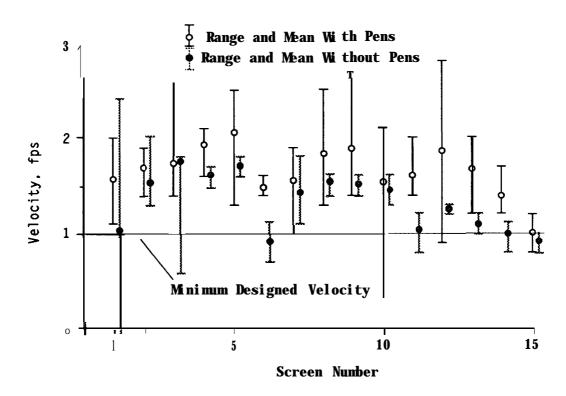


FIGURE 13. Sweep Velocity at 0.8 of the Depth in Front of Drum Screens at the Wapato Canal, Spring 1989

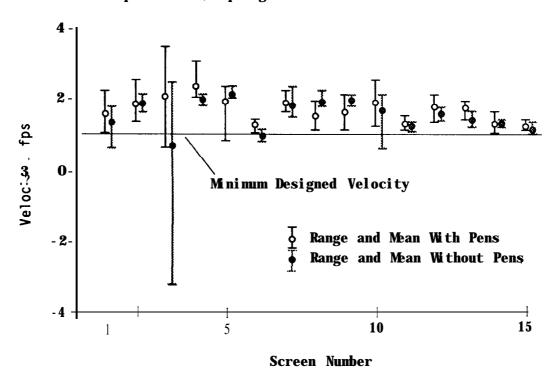


FIGURE 14. Sweep Velocity at 0.8 of the Depth Under the Curvature of Drum Screens at the Wapato Canal, Spring 1989

TABLE 1. Approach Velocities (fps) at the Head of Fish Bypasses at the Wapato Canal, Spring 1989

	0.3	Depth	0.8 Depth			
Bypass #	With Pens	Without Pens	With Pens	Without Pens		
1	1. 57	1. 76	1. 56	1. 28		
2	1. 79	1. 97	1. 57	1. 25		
3	1.68	1. 79	1.44	1. 21		

CHANDLER SCREENS

Velocity measurements varied throughout the facility. The variability resulted in measurements being different from the design criteria.

Approach velocity exceeded 0.5 fps by more than 10% at 12 of the 76 measurement locations (Table 2). Most of the high approach velocities occurred under the curvature of the drum screens at 0.8 and 0.9 of the depth. Approach velocity was low in front of screens at the upstream end of the facility but nearly equal to the 0.5-fps standard in front of screens at the downstream end of the facility. Wing walls had little affect on approach velocity.

Sweep velocity resulting in less than a 2:1 sweep-to-approach ratio occurred at 13 (17%) of the 76 measurement locations, and was <1.0 fps at 40 (53%) locations. Low sweep velocity was most evident at 0.9 of the depth. Sweep velocities under the curvature of the drum screens at 0.8 of the depth were comparable to sweep velocities measured in front of the drum screens; however, the high approach velocities under the curvature of the drum screen resulted in a poor sweep-to-approach ratio. Sweep velocity was low in the upstream third of the facility, highest in the middle third of the facility, and slightly reduced in the downstream third of the facility.

Vertical velocity was generally low throughout the facility. Disruptions in flow associated with vertical movement of water, such as upwelling and swirling, were not evident during our sampling.

Flow through the terminal fish bypass (bypass 3) was lower than through the two intermediate bypasses, based on sweep velocity measurements taken in the entrance of the three fish bypasses (Table 3). Additionally, overall fish bypass flow was less than is specified in the operating criteria. Only two of the four pumps in the separation chamber were operating during our measurement series.

TABLE Summary of Approach (X), Sweep (Y), and Vertical (Z) Velocity Measurements (fps) in Front of the Drum Screens at the Chandler Canal. Summer 1989

		0.2			0.8			0.05			0.5			0.8(a)	<u> </u>		0.9(a)	
Scre	enX	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z	X	Y	Z
1	0.10	0.48	-0.06	0.20	0.33	-0.02												
2	0.10	0.60	-0.09	0.10	0.55	-0.03												
3	0.11	0.71	-0.13	0.13	0.62	-0.04												
4	0.18	0.86	-0.07	0.19	0.72	-0.01												
5	0.20	0.87	-0.12	0.20	0.75	-0.03												
6	0.20	0.90	-0.11	0.21	0.78	-0.05												
7	0.29	0.97	-0.09	0.27	0.73	-0.01	0.24	0. 92	- 0. 09	0.27	0.88	-0.08	0.70	1.82	-0.12	0.35	0.58	0.13
8	0.30	0.92	-0.12	0.28	0.68	-0.02	0.29	0. 94	-0.17	0.28	0.79	-0.07	0.76	1.79	0.29	0.38	0.43	0.10
9	0.35	1.10	-0.11	0.39	0.77	0.05	0.30	1.14	-0.09	0.37	1.02	-0.14	0.79	1.69	-0.38	(b)	(b)	(b)
10	0.30	1.17	-0.13	0.34	1.16	-0.10												
11	0.30	1.23	-0.13	0.30	1.10	-0.06												
12	0.30	1.27	-0.10	0.30	1.07	-0.04												
13	0.30	1.04	-0.12	0.30	1.07	-0.04												
14	0.30	1.24	-0.10	0.30	1.00	-0.01												
15	0.40	1.02	-0.06	0.32	0.98	0.02	0.31	1.27	-0.08	0.36	1.12	-0.04	0.48	1.08	0.09	0.50	0.77	0.10
16	0.40	1.18	-0.03	0.32	0.91	0.33	0.40	1.14	-0.06	0.39	1.06	0.04	0.58	1.19	0.13	(b)	(b)	(b)
17	0.50	1.27	-0.12	0.74	0.86	-0.06	0.50	1.26	-0.10	0. 59	0.88	-0.17	0.83	0.92	-0.15	0.83	0.63	0.01
18	0.39	1.18	-0.13	0.49	0.98	-0.05												
19	0.41	1.17	-0.12	0.48	1.02	-0.08												
20	0.40	0.99	-0.12	0.48	0.94	-0.07												
21	0.40	1.25	-0.12	0.52	0.80	-0.06												
22	0.50	1.05	-0.11	0.54	0.65	-0.01	0.40	1.15	-0.10	0.48	0.90	-0.06	0.67	0.97	-0.07	0.74	0.58	0.08
23	Not in	opera	tion															
24	0. 49	0. 98	-0.10	0.50	0.94	-0.02	0.50	1.21	-0.10	0.51	1.03	-0.05	0.70	1.16	-0.01	0.69	1 .Ol	0.10

⁽a) Measurement made under curvature of the screens: all others made in front of screens.

⁽b) Obstruction under the screens: no data.

TABLE 3. Summary of Approach (X), Sweep (Y), and Vertical (Z) Velocity Measurements (fps) at the Entrance to the Fish Bypasses at the Chandler Canal, Summer 1989

		0.7 Depth		0.	8 Depth	
Bypass	X	Y	Z	X	Ÿ	Z
1	- 0. 06	1.98	0.11	0.24	1.18	0.21
2	- 0. 11	1. 73	0.19	-0.23	1.49	0. 31
3	0.06	1.38	0.24	-0.54	1.26	0.47

Sweep velocity in the upstream end of the separation chamber is surfaceoriented (Figure 15, Table 4). Sweep velocity at 0.8 of the depth increases from zero at the upstream end of the separation chamber to about 60% of the sweep velocity at 0.2 of the depth near the entrance to the fish return slot. Based on the cross-sectional area in the fish return, the fish return flow was about 25 cfs, with slightly more water entering the fish return from the surface.

Approach velocity was less than 0.5 fps at the face of the first traveling screen (Table 5. Figure 16). The lack of sweep velocity at 0.8 of the depth observed in velocity measurements in the upstream end of the separation chamber persisted in front of the first traveling screen. Because of limited accessibility, no measurements were taken in front of the second traveling screen.

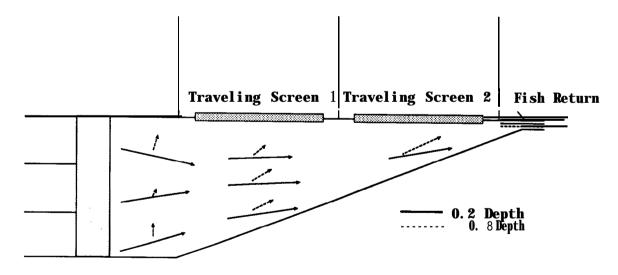


FIGURE 15. Flow Patterns (Plane View) in the Chandler Screens Separation Chanber as Described by Velocity Data and Visual Observations of the Water Surface

TABLE Summary of Approach (X), Sweep (Y), and Vertical (Z) Velocity Measurements (fps) in the Separation Chamber and Fish Return at the Chandler Canal, Summer 1989

		0	.2 Dept	h).8 Depth	
Transect ^(a)	Position(b)	X	Y	Z	X	Y	Z
Upper	Outer	0.52	1.67	-0.39	0.28	0.0	- 0. 01
	Center	0.19	1.76	-0.20	0.18	0.01	-0.20
	Inner	- 0. 41	1.90	-0.36	0.40	0.01	-0.18
Screen 1	Outer	0.20	1.84	-0.31	0.27	0.53	-0.25
	Center	0. 09	1.87	-0.27	0.30	0.49	-0.08
	Inner	0.07	1.66	-0.20	0.37	0.32	-0.06
Screen 2	Center	0. 29	1. 64	- 0. 21	0.46	0.99	-0.18
Fish Return	(c)	0.01	1.75	-0.04	0.02	1.33	0.04

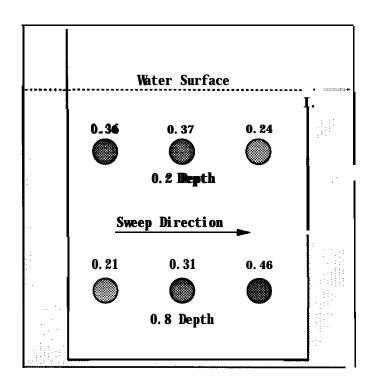
Upper transect is across the separation chamber upstream of the first traveling screen: Screen 1 and Screen 2 transects are adjacent to the centerline of each screen.

TABLE 5. Summary of Approach (x). Sweep (Y). and Vertical (Z) Velocity Measurements (fps) at the Face of the First Traveling Screen at the Chandler Canal, Summer 1989

Position	0.	2 Deoth		0	.8 Depth	
	X	Y	Z	X	Ÿ	Z
Upper	0.36	1. 09	0.27	0.21	-0.05	0.29
Center	0.37	0.88	0.05	0.33	-0.17	0.43
Lower	0.24	0.86	0.06	0.46	-0.13	0.19

Outer position is 1 ft from the outer wall: center position is midway between the outer wall and the catwalk in front of the traveling screens; inner position is adjacent to the catwalk, about 5 ft from the face of the traveling screens.

Measurements were taken at the centerline of the fish return slot near the entrance.



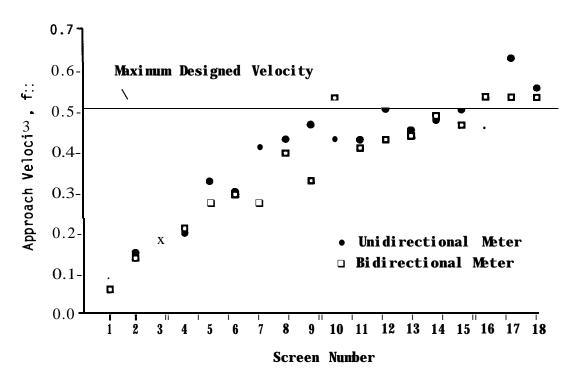
FIGURF 16. Approach (Impingement) Velocity at the Face (Side View) of the First Traveling Screen in the Chandler Screens Separation Chamber

EASTON SCREENS

The low flow through drum screens at the upstream end of the Easton Screens indicates that porosity boards are needed to balance flows. Flow through the screens may be partially attributable to water flow around a bend in the canal upstream of the screens forebay that results in high sweeping velocity along the outer wall of the screens forebay.

Velocity measurements taken on June 14 with a unidirectional water current meter and on June 15 with a two bidirectional (Figure 17) water current meters produced similar results. Overall, velocities measured with the unidirectional meter were slightly higher than the velocities measured with the bidirectional instruments: however, the difference may be a result of the maximum stable reading observed with the unidirectional meter, which was recorded for the data set, while ten velocity readings with the bidirectional meters were averaged to produce the data set.

Velocity through the drum screens was lowest through the screens at the upstream end of the facility and steadily increased throughout the length of the facility. The highest velocities were observed at the last three screens (Screens 16 through 18). Velocity across the screen face has little meaning because the velocity measurements were made in the screen bays behind the drum screens.



FIGURF 17. Velocity Measurements to Evaluate Flow Balance Through the Drum Screens at the Easton Canal, Summer 1989

DISCUSSION

The measurement objectives were different at each screen facility. At Wapato, approach and sweep velocity measurements were taken to evaluate the effect of rearing pens in the screen forebay. At Chandler, approach, sweep, and vertical velocity measurements were taken in front of the rotary drum screens. Velocities were also measured at the entrance of fish bypasses, in front of traveling screens in the separation chambers, and in the entrance to the fish return. At Easton, velocity was measured behind the screen to provide information for designing porosity boards to balance flow through the screens.

EFFFCT OF SALMON-REARING PFNS ON VEIOCITY MEASUREMENTS AT THE WAPATQ SCREENS

Velocity measurements taken at the Wapato Screens before and after the removal of the YIN salmon-rearing pens show that the pens can affect both the magnitude and stability of water velocity in front of the drum screens. Approach and sweep velocities were erratic in front of the drum screens when the pens were in the forebay and stable after the pens were removed. The magnitude of approach velocity at the screen face was not affected; however, the sweep velocity was less at 0.2 of the depth and greater at 0.8 of the depth when the pens were in place.

The unstable velocity readings we observed are believed to be the result of swirling water moving along the face of the drum screens, based on visual observations made during data collection. Swirling water could result in intermittent high impingement velocities for small fish as the swirl moves along the face of the screens: however, no fish impingement was observed on drum screens adjacent to the rearing pens in screen integrity tests conducted in 1988 ((Neitzel et al. 1990b).

Velocity measurements taken at the Wapato Canal with the rearing pens in the screen forebay did not compare well with data collected in 1988 (Abernethy et al. 1989) under similar canal flow and operating conditions. Factors that might have caused differences in the two data sets are

- . differences in sedimentation in the screen forebay
- the location and number of inoperable screens when the measurements were made
- the degree of algal fouling on the screen panels in the rearing pens day-to-day variation of hydraulic conditions within the canal.

The greatest discrepancies in velocities between the two data sets occurred in measurement locations that were adjacent to inoperable screens or wing walls.

VEIOCITY CHARACTERISTICS AT THE CHARDIER SCREEJJ

Water flow in the Chandler Screens forebay was very uniform, based on visual observation. Few current lines or swirls were visible. However, it appeared that the canal forebay is too wide to maintain an adequate sweeping velocity in front of the screens. Additionally, our velocity measurements indicated that porosity boards will probably be required to achieve more flow through the drum screens at the upstream end of the facility.

Low flows through drum screens at the upstream end appear to be a common problem at screening facilities with the drum screens installed at an angle to canal flow. Modification in hydraulics resulting from installation of porosity boards may be partially responsible for increased turbulence in the screen forebay.

Based on velocity measurements at the entrance of each of the three fish bypasses and in the separation chamber. fish return flow did not meet design criteria specifications. Although approach velocities did not exceed 0.5 fps during our data collection, only one of the two pumps behind each screen was operating. During four-pump operation of the separation chamber, impingement velocities could increase substantially at the face of the traveling screens.

FLOW BALANCE AT THE EASTON SCREENS

The low flow through drum screens at the upstream end of the Easton Screens indicates that porosity boards are needed to balance flows. Poor flow through the screens may be partially attributable to water flow around a bend in the canal upstream of the screen forebay that results in high sweeping velocity along the outer wall of the forebay. Porosity boards were installed following our measurement series, and flow balance through the screens was improved (Hosey & Associates 1989).

SUMMARY

Velocity measurements were conducted at three fish screening facilities in the Yakima River Basin: the Wapato, Chandler, and Easton Screens. Our objective at the Wapato Screens was to determine if the salmon-rearing pens in the forebay adversely affected flow parameters in front of the drum screens. At the Chandler Screens, our objective was to determine if velocity parameters in front of the rotary drum screens and within components of the fish bypass system were consistent with design specifications necessary to provide effective fish bypass. The objective of flow measurements at the Easton Screens was to determine where porosity boards were needed to equalize water flow through the drum screens.

WAPATO SCREENS

Velocity measurements taken before and after the removal of three salmon-rearing pens from the screen forebay indicated that although the pens had only a minimal effect on actual approach and sweep velocities at the face of the drum screens, the pens contributed to increased turbulence and instability of the water flow. Swirls and turbulence at the face of drum screens could result in intermittent increases in approach velocities. The net pens did not appear to affect flows through the three fish bypasses.

CHANDLER SCREENS

Approach velocity was low in front of the drum screens at the upstream end of the facility but steadily increased in front of drum screens at the downstream end of the facility. Porosity boards are needed to balance flow through the array of screens.

Sweep velocity was generally low in the Chandler Screens forebay, especially under the curvature of the drum screens. Low sweep velocities and elevated approach velocities under the curvature of the drum screens result in velocity conditions that do not meet the design criteria standards.

Flow through each of the three fish bypasses were less than specified in the operating criteria. Sweep velocity in the separation chamber was generally low. Approach velocity at the face of traveling screens in the separation chamber were within design criteria guidelines; however, only two of the four bypass pumps were operating when the measurements were taken. Flow out the fish return pipe appeared to be adequate.

EASTON SCREENS

The low flow through drum screens at the upstream end of the Easton Screens indicates that porosity boards are needed to balance flows. Poor flow through the screens may be partially attributable to water flow around a bend in the canal upstream of the screen forebay that results in high sweeping velocity along the outer wall of the forebay. Porosity boards were installed following our measurement series, and flow balance through the screens was improved (Hosey b Associates 1989).

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APPENDIX 4

OPERATING CRITERIA FOR THE WAPATO. CHANDLER. AND EASTON FISH SCREENING FACILITIES

APPFNDIX A

OPERATING CRITERIA FOR THE WAPATO. CHANDLER. AND EASTON FISH SCREENING FACILITIES

This appendix contains the operating criteria for the three fish screening facilities included in this report. The criteria were developed by hydrologists from the National Marine Fisheries Service. The intent of the criteria is to provide the information necessary so that maintenance personnel can set and adjust fish bypass flows to achieve optimum fish bypass conditions at each screening facility.

The operating criteria for the Wapato Screens are provided on pages A.2 through A.5. Text describing the operating criteria appears on pages A.2 through A.3. and a diagram of the Wapato Screens is shown on page A.4. A graph summarizing weir crest height adjustment based on canal surface elevation is shown on page A.5.

The operating criteria for the Chandler Screens are provided on pages A.6 through A.13. Text describing the operating criteria appears on pages A.6 through A.8. Pages A.9 through A.11 describe weir gate adjustments for three ranges of canal water surface elevations. Page A.12 contains a graph showing the appropriate weir crest elevations for a range of canal water surface elevations. Page A.13 shows the appropriate surface levels for controlling flow through the Juvenile Evaluation Building.

The operating criteria for the Easton Screens are provided on pages A. 14 through A. 16. Text describing the operating criteria appears on pages A. 14 and A. 15, and a diagram of the Easton Screens is shown on page A. 16.

Operating Criteria Wapato Canal Fish Screens Bypass System

Operation of the bypass system requires the adjustment of four 2-foot wide bypass overflow weir gates (these are temporarily stoplogs at the present time) located in the fish bypass channels and two S-foot wide excess water overflow gates located behind the pumps in the pumpback structure. These weir gates (or temporary stoplogs) control the quantity of bypass flows and the water surface elevations within the system for good fish passage.

Weir gates (or stoplogs) should be adjusted as follows. Weir gate locations are shown on the attached sketch.

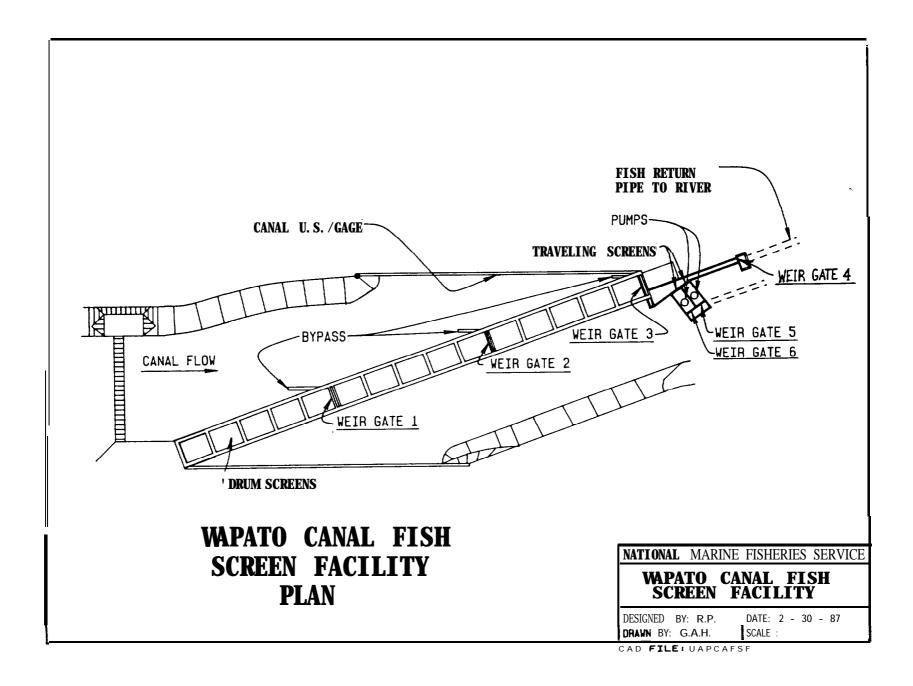
Normal Operation (no pumpback):

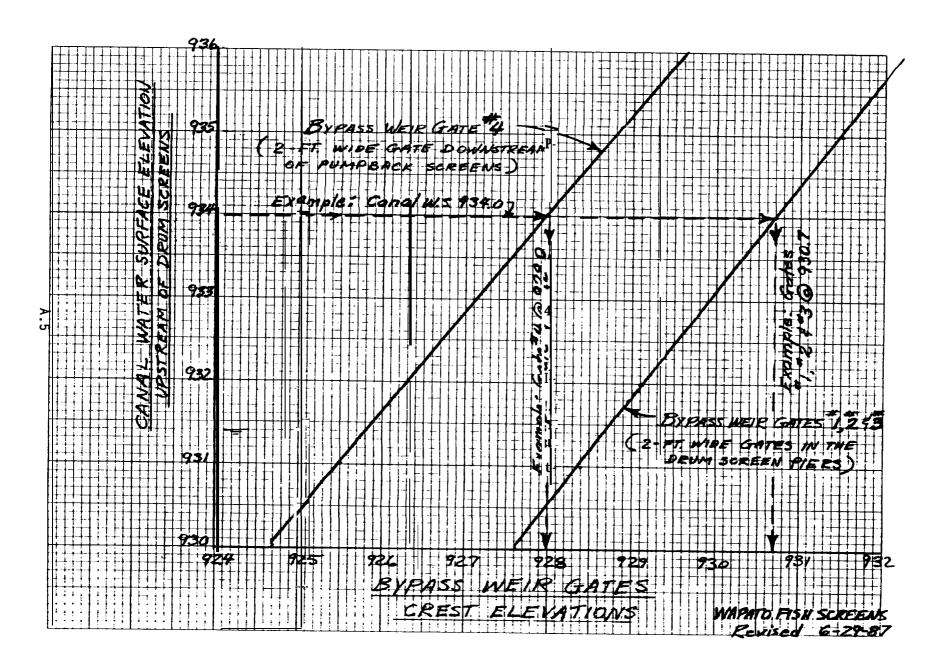
- 1. Adjust crest of weir gates #1, #2, and #3 (or top of temporary stoplogs) to appropriate elevation depending on canal W.S. (water surface) elevation from attached graph. Example: canal W.S. in front of drum screens is at elevation 934.0; set crest of weir gates (stoplogs) to elevation 930.7.
- 2. Adjust crest of weir gate #4 (or top of temporary stoplogs) to appropriate elevation depending on canal W.S elevation as shown on attached graph. Example; canal W.S elevation 934.0; set crest of #4 weir gate (or top of stoplog) at elevation 928.0.
- 3. Adjust weir gates #5 and #6 "equally" until W.S. elevation in front of traveling screens is 3.5' lower than canal W.S elevation in front of drum screens. Example: canal elevation 934.0: adjust weir gates #5 and #6 equally until W.S. elevation in front of traveling screens is 930.5.

Oweration with Pumwback;

1. Set weir gates #1, #2, #3, and #4 same as for Normal Operation (No Pumpback).

- With either one or both pumps in operation adjust both weir gates #5 and #6 to maintain the traveling screen W.S. 3.5' lower than canal W.S. elevation. Divide flow through both traveling screens equally.
- 3. If the difference between the canal W.S. and the traveling screen W.S. is greater than 3.5', even with both weir gates #5 and #6 closed, then lower gates #1, #2, & #3 equally to obtain 3.5' difference. Note: This is very important since for certain conditions the pumps may have enough capacity to pull down the water level in the pumpback structure down too low, drying up the bypass flow over weir gate #4 and resulting in major fish damage.





OPERATING CRITERIA CHANDLER SCREENS

3-2-87

- 1. Check canal water surface elevation.
- 2. Locate canal water surface on the Weir Gate Operation graph (see the horizontal line). Imagine, or draw lightly, a line upward on the graph from that point. It will intersect the GATE NO. 4 and the GATE NO. 1,2, and 3 lines. Then read horizontally to the left from the point of intersection, and read the required weir crest elevations.
- 3 Set GATE NO. 4 to the appropriate weir crest setting from the graph.
- 4. Set GATE NO. 1,2, & 3 to the appropriate setting from the graph.
- 5. Set the pump structure water surface to the appropriate level:

PUMPBACK MODE

Set the 4 pump discharge pipelines so the flow meters each read 25 cfs. Check these readings once every few months of operation.

GRAVITY MODE

Hand set each of the two gravity bleed-off gates until the pumpback structure water surface is:

(For canal water surface of El. 630.9 and higher)-E1.627.8

(For canal water surface of El. 630.7)-El. 627.6

(For canal water surface of El. 630.5)-El. 627.3

(For canal water surface of El. 630.3 and lower)-El. 627.0

NOTE: When in the gravity bleed-off mode, bleed-off gates should be set at equal openings, which will draw equally through each traveling screen.

6. Checks:

Check the downwell staff gauge reading for each of the 3 bypass downwells. Remove floating debris. If the bypasses are not impeded, the three bypass downwell readings should be the same (within 0.2'). Check the pump structure bypass downwell reading. It should be at El. 626.0 in order to pass the required flow to the evaluation building.

STANDARD OPERATING PROCEDURES CHANDLER SCREENS

2-3-87

I. OPERATIONS:

- A. NONE-SAMPLING MODE:
 - 1. General

During this mode of operation, bypass flow is being routed directly to the river rather than through the sampled facilities of the juvenile evaluation building.

There are five gates which must be properly set in order for the three main screen and one secondary screen bypasses to function as designed. Gates 1,2, & 3 are the weir gates in the pumpback structure, which control flow in each of the main bypasses. Gates 4 is the weir gate, which controls flow into the secondary bypass and the water surface in the pump structure pool.

Gate 5 is the bulkhead gate in the downwell of the evaluation building, which should be set initially, then not reset until evaluated at a later date.

The settings of Gates 1-4 are based on the canal water surface elevation. The attached graph indicates the weir crest elevation (top of weir) that is required for a given canal water surface. After taking the canal water surface reading, set Gates 1-4 as indicated on the graph. Be sure to allow a minimum of 10 minutes for flow conditions to reach equilibrium.

2. OPERATIONS AND TROUBLE SHOOTING: Gates 1-3
Staff gages are installed to aid in verifying water
surface elevations through the system, and for the
purpose of identifying when blockages may be inhibiting
flow. A staff gage should be located in a forebay
location that is easily viewed from the catwalk on the
main screen structure. Staff gages should also be
located on the upstream wall of each of the upwells in
the pump structure. Check the differentials from
forebay to each upwell. This value should be between
2' and 3', depending on the forebay water surface.
There will be surging in the upwell, so take the
average reading between high and low surfaces. The
IMPORTANT thing is that the differential readings are

within **0.3'** of each other. If one reading is more the 0.5' lower than the other two, then the weir gate is improperly set or there is a blockage in one of the bypasses.

3. OPERATIONS AND TROUBLE SHOOTING: Gate 4
There should also be staff gages in the main pumpback structure pool and the secondary bypass downwell.
During normal operating periods, the secondary downwell gage reading should ALWAYS be 626.0. Adjustment of Gate 4 as indicated on the attached graph should assure the reading.

The water surface elevation in the pumpback structure pool is controlled **by** the pump discharge (or gravity pipe discharge) and the Gate 4 flow. The pump discharges will be set initially, then left unchanged.

The water surface elevation in the pumpback structure should be 627.8 at all canal surface elevations above 630.9. Between canal elevations 630.9 and 630.4, the pumpback surface will drop to 627.0. Gate 4 adjustment, as shown on the graph, is necessary to maintain the required bypass flow to the juvenile facility.

B. SAMPLING MODE- Switching to and from:

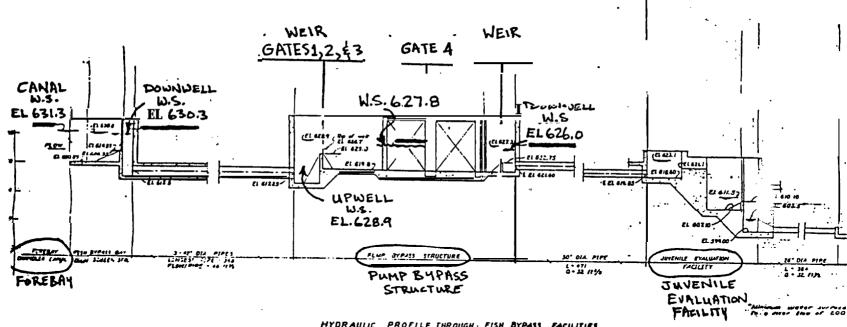
In the juvenile evaluation facility upwell, there are two weir gates, which do nothing except control the direction of flow. One should always be fully open and the other should always be closed. The only exception is during switching from one mode of operation to the other. ALWAYS remember that the correct procedure is to open the other gate prior to closing the first gate. Otherwise, the upwell will overtop.

II. MAINTENANCE:

- 1. Keep all gages clean. They should be readable in order to insure correct operation of the facility.
- 2. Check all 4 bypasses for accumulations of floating debris. Remove especially debris that may become blocked in the bypasses.

Note: Questions or comments, call Steve Raney. Remember, this is a preliminary set of criteria.

CANAL WATER SURFACE = 631.3 Top of weir Gates 1,2, 43 = EL 626.7
Top of weir Gate 4 = EL. 624.85

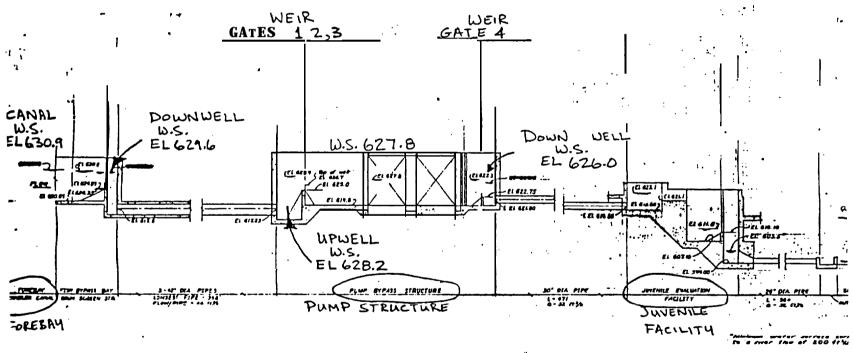


HYDRAULIC PROFILE THROUGH - FISH BYPASS . FACILITIES

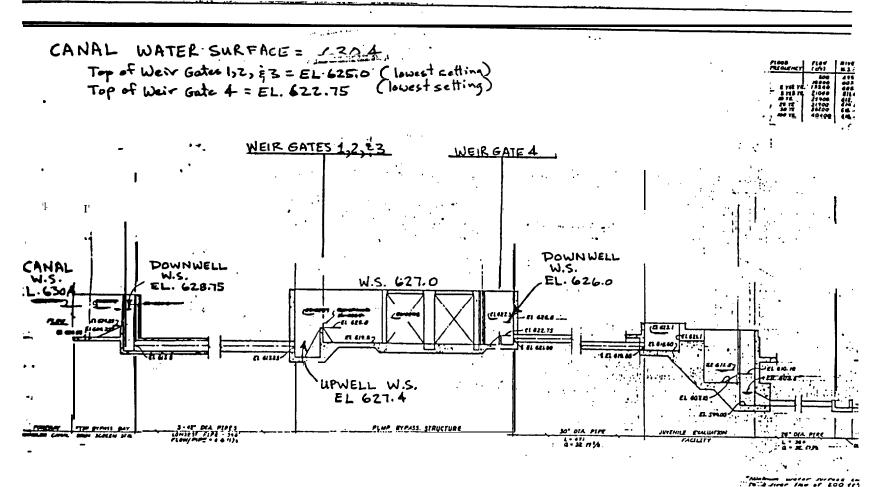
CANAL WATER SURFACE = 630.9

Top of Weir Gates 1,2, &3 = EL 625.0 (lowest setting) Top of Weir Gate 4 = EL. 624.85

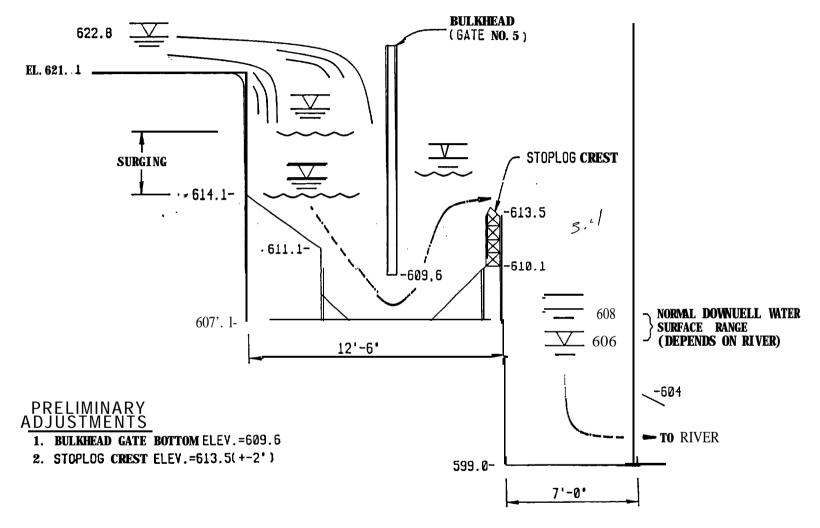
(01)	# 1 2 C
200 2300 2300 2100 31700 31700 30100	4023 4088 6114 611.7 64.8 64.8
	(di) 000 0000 13300 21000 21700 31700 34100



HYDRAULIC PROFI LE THROUGH - FISH BYPASS FACILITIES



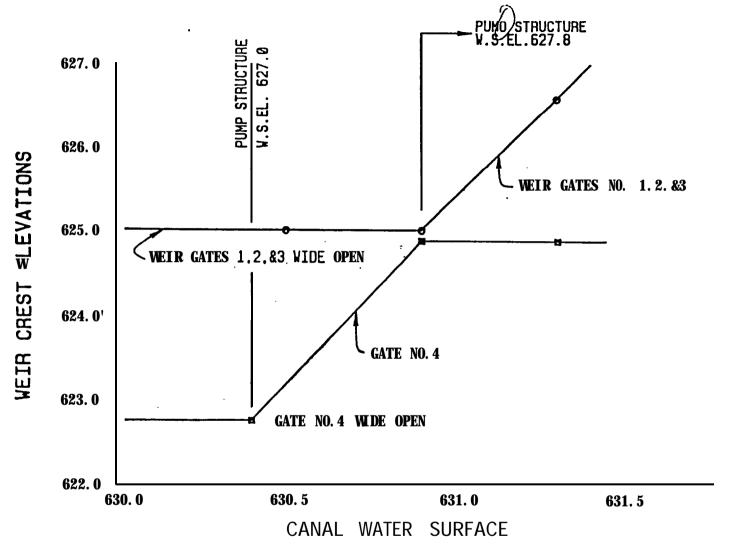
HYDRAULIC PROFILE THROUGH - FISH BYPASS FACILITIES



CHANDLER SCREEN JUVENILE EVALUATION BUILDING

(BYPASS MODE)

BYPASS DOWN .L N. M F. S. 2-Z-87



GATE NO'S 1.2.&3 PASS 44 CFS EACH GATE NO.4 PASSES 32 CFS

CHANDLER SCREEN
WEIR GATE OPERATION
N. M. F. S. 2-3-87

KITTITAS CANAL SCREEN/BYPASS OPERATING CRITERIA (NMFS - 7/6/89)

Comments on screen and bypass operation:

- 1. There is no canal water surface elevation (WS) control structure to maintain screen submergence.
- 2. The bypass design flow is **80** cfs. The system is designed to pass **80** cfs even at low canal WS elevations.
- 3. During periods of minimum stream releases past Easton, total bypass flow should not be reduced below 40 cfs.
- 4. Based on the need for coordinating adult and juvenile passage facilities flow releases, relative to the Bureau's Easton gage reading, the correct mode of operation during low streamflow periods is based on the June 15 date. Prior to that date, juvenile passage is emphasized; after June 14, adult passage is emphasized.
- 5. Bureau miscellaneaous flows at the dam equal 15 cfs \pm . These are not considered below, but do take priority.

PRIOR TO JUNE 15: (Emphasis - juvenile passage)

1. Easton Gage reading less than 105 cfs:
 Bypass flow = (Easton gage flow) - (Easton ladder
 flow of 28 cfs)

Set gates G-1 and G-2 5.0 feet **below** the canal WS. Set Gates G-3 and G-4 as follows:

If bypass flow to be 40 cfs, set weir gate crest 1.3 ft. below upwell WS.

If bypass flow to increase from 40 to 80 cfs, increase weir gate crest submergence incrementally from 1.3 to 2.1 ft. below upwell WS.

Set gate G-5 at the following crest elevation: If canal WS is above el. 2175: crest el. = 2169.0

If canal WS is below el. 2175: set gate at lowest setting.

Set gate G-6 at crest elevation 2162.0.

2. Easton Gage reading greater than 105 cfs: Set Gates G-l and G-2 5.0 feet below canal water surface.

If bypass flow to \mathbf{be} between 40 and 80 cfs, increase weir gate crest submergence incrementally from 1.3 to 2.1 ft. below upwell WS.

Set gate G-5 at the following crest elevation: If canal WS is above el. 2175: crest el. = 2169.0

If canal WS is below el. 2175: set gate at lowest setting.

Set gate G-6 at crest elevation 2160.9.

AFTER JUNE 14: (Emphasis - adult passage)

1. Easton Gage reading less than 160 cfs: Gates G-l and G-2 set at 5.0 feet below the canal water surface elevation.

Gates G-3 and G-4 set at 1.3 ft. below upwell water surface (40 cfs).

Remaining flow through fish ladder (up to 120 cfs). Set gate G-5 at the following crest elevation:

If canal WS is **above** el. 2175: crest el. = 2169.0

If canal WS is below el. 2175: set gate at lowest setting.

Gate G-6 set at crest elevation 2162.0.

2. Easton Gage reading greater than 160 cfs: Gates G-l and G-2 set at 5.0 feet below the canal water surface elevation.

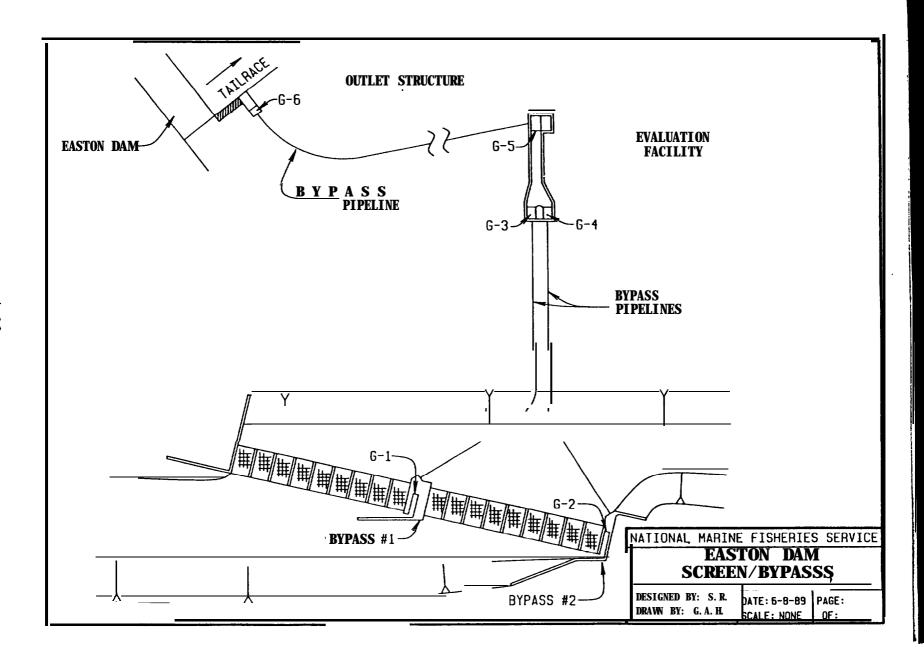
Gates G-3 and G-4 set for bypass flow between 40 and **80** cfs: Increase G-3 and G-4 wier crest submergence below upwell WS incrementally from 1.3 to 2.1 ft.

Set gate G-5 at the following crest elevation:

If canal WS is above el. 2175: crest el. = 2169.0

If canal WS is below el. 2175: set gate at lowest setting.

Gate G-6 set at crest elevation 2160.9.



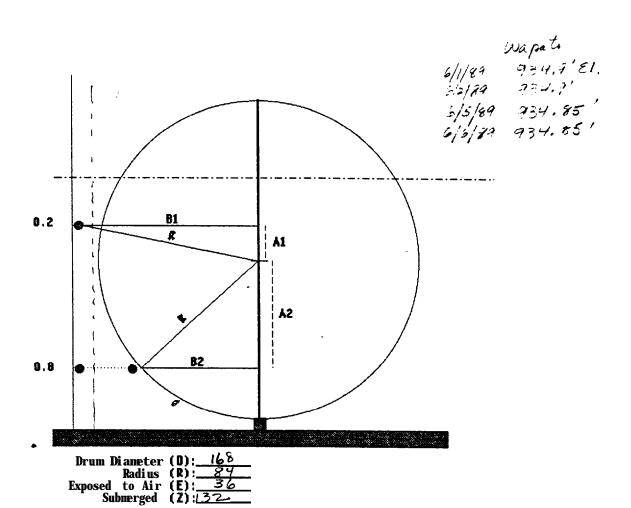
APPFNDIX B

WAPATO SCREENS RAW DATA SHEFTS

APPENDIX B

WAPATO SCREENS RAW DATA SHEETS

This appendix contains the raw data sheets for flow measurements taken at the Wapato Screens on June 1 and 2 and June 5 and 6, 1989. Page B. 2 shows the calculations made to position probes at the proper depths and the distance between the probe and the screen face at each depth. Raw data for measurements taken before the Yakima Indian Nation salmon rearing pens were removed from the forebay are presented on pages 8.3 through 8.20. Raw data for measurements taken after the rearing pens were removed from the forebay are presented on pages 8.21 through B.38.



Distance From Vertical to Screen Face

0.2 Z: R-B1= 2.92"

0.8 Z: R-B2= 22.86"

Note: same measure ment depths were used for series on 6/5-6/1/89, despite the canal elevation being 0.05' lower - WA

	Total Forebay D Screen Diane Screen Exp Screen Subme	Date: _ Personnel: _	6-1-59 CSA 000	
	6	<u>-1</u> .	<u>6 ·</u>	2
Time Start	1601	1601	1017	1017
Ti ne End	1605	1605	1020	1020
Depth Vector 1 2 3 4 5 6 7 8 9	0.2 S A 0.6 -0.3 0.9 0.2 1.3 0.9 0.8 -0.1 0.8 0.1 0.7 0 1.0 0.4 0.9 0 1.0 0.5	0.8 S A 1.8 0.8 1.8 1.1 1.1 -0.6 1.3 0.2 2.0 1.3 1.7 0.7 1.6 1.0 1.9 0.6 1.4 0.7 1.9 0.8	0.8a S - A 1,2 - 0.6 2 - 0.5 2,2 - 0.6 1,9 - 6.6 1.4 - 0.7 1,0 - 0.7 1,2 - 0.9 1.4 - 0.9 1.3 - 0.6	0.8 S = A 0.9 -0.4 1.5 -0.5 1.5 -1.2 1.4 -1.0 1.1 -0.9 1.0 -0.8 1.3 -0.8 1.3 -0.8
Average M ni mum Maxi mum	0.88 0.15	1.58 0.60	1.5 3 0.73 1.0 3.5 2.2 0.9	1.25 0.77 0.9 0.4 1.5 1.2

Notes:

.

Screen # 2		Personnel:	CSA DDD	
			2.2	
Time Start	552	1552	1006	1006
Time End	<u> </u>	1555		
Depth Vector 1 2 3 4 5 6 7 8 9	0.2 S A 1.2 0.7 1.4 0.3 1.0 0.2 1.4 0.3 1.3 0.4 1.1 0.2 1.1 0.2 1.2 0.3	1.6 0.5 1.6 0.6 1.2 0.4 1.6 0.9 1.4 0.3 1.6 0.4 1.9 0.2 1.7 0.2	0.8a S -A 1,6 -0.5 1.6 -0.9 1.6 -0.9 1.7 -0.5 1.8 -0.9 1.6 -0.7 2.0 -0.8 2.5 -0.5 1.7 -0.9	0.8 S - A 1.0 - 0.2 1.3 0.5 1.2 - 0.2 1.4 - 0.4 1.7 - 0.2 1.0 - 1 5 1.4 - 2.0 1.6 0.6 16 + 0.4
10	1.2 63	9.0	2,0 I - 0.7	1.8 0.2
Average Minimum	1.19 0.25	1,68 0.49	1.8/ 0.54	1.40 0.28
Maxi mum	1, 0,0	1,9 0.9	2.5 0.8	1.8 2.0

Screen <u>#</u> 3	Scree	n Diamet en Exnos	er (10.) ed (in.)	3.6	Pe	Date: _ ersonnel: _	6 - r- CSA11	6-Q 000
		6.	(_6_	2	
Time Start	1537		153	7		Sf	958	`
Time End	154,	1	154		13)	100	1
Depth	0.	2		0.8		0.8a		0.8
Vector	S	A	S	A	S	- A	S	- A
1	ルタ	4.2	1,0	2.0	1,7	-04	/· s	-0.5
2	1, 7	0.3	2.0	0.6	2.4	-1,2	1.4	- 0.9
3	1.6	0.2	1.6	0.5	1. 3	-07	1.1	- 0, 2
4	2.2	0.8	1.5	-0.6	0.6	-0,5	2.1	-1.0
5	1.7	0 · 3	1.6	~ 0.4	0,8	- 0. 4	2.0	-0.7
6		-0.4	2.6	1.9	3, 4	-1.2	0.9	0.8
7	1.3	0.4	114	-/, 3	3.6	- /.0	07	7.3
8	1.4	0.1	1.8	2.3	1,6	-0,4	1. R	- 6. 3
9		-0.6	1.4	0.5	3.2	-09	/ 0	- 2.4
10	1.5	0.2	1.9	1.7	2,7	-0.4	1.4	1-0.3
	1 1 60 1	A 16	1,74	0.57	2.03	1 6 7 1	1 2/2	10//2
Average	1.52	0.15.	1.4			0.71	1.39	0.42
Mi ni mum	1.5		<u> </u>	-1.3	0.6	0.4	0.7	-1.3
Maxi mum	2.レ	0.8	2.6	2.3	3.4	1.2	2./	2.4

Screen #	Total Forebay I Screen Dia Screen Ex Screen Subm	Date: _ Personnel: _	6-1. 89 CEA/DOD	
Time Start	1528	1528	945	945
Time End	1532	1532	948	948
Ocath				
Vector	0.2 T S T A	0.8 S I A	0.8a	0.8
VECTOR	1 1. £ 1 0.3	1,9 -0.4	S - A	S - A
2	I 1. 2 0 · 3	3.1 2.3	2 2 - 0.6	1.4 -1.7
3	, I 0.3	1.8 0.2	2.2 0.2	1.5 -04
4	1 / 6 0 3	2.) 2.2	2.0 -0.6	19 -02
5	1.7 0.2	1.6 0.3	2,5 -0.6	1.8 -0.7
6	1,9 0.5	1.9 1.1	2.6 -0.7	1.6 0.3
7	1,8 0.2	2.0 1.7	2.1 -0.2	1.7 -0.1
8	1.6 0.2	1.8 0.4	2.3 -0.7	1.7- 0.8.
9	1.8 0.3	2.1 0.9	2.3 -0.8	1.4 -0.9.
10	1.7 0.3	2.0 1.9	3.0 -1.1	1.6 -1.4
Average	1.74 0.29	1.93 1.06	2.31 0.61	1.65 0.48
Mi ni mum	1,6 0.2	16 -04	2.0 0.2	1.4 -0.3
Maxi mum	1.9 0.5	2.1 2.3	3.0 1.1	1.9 1.7

Screen #	Scre Scr	en vramet een Exnos	oth (in. er (in.) sed (in.) ged (in.)	36	Pe	Date: _ rsonnel: _	6-1- CSA)(\$9 000
		6.0				<u>6 ·</u>	2	
Time Start Time End	152		152		9 9	37 40	93	
Depth Vector 1 2 3 4 5 6 7 8 9	S 1.9 1.4 1.5 2.0 1.6 1.9 1.7	0, 2 A 0 2 6 3 0 3 0 3 0 2 0 2 0 2 0 3 0 3 0 3	S 2.3 2.3 1.3 2.4 1.9 2.2 2.4 1.8 2.5	0.8 A 0.9 6.5 -1.4 1.2 0.2 -0.4 1.8 -0.6	S 2.3 2.7 2.7 2.1 0.8 2.0 1.3 2.1 2.3 1.6	0.8a - A - 0.3 - 0.1 - 0.9 - 0.9 - 0.7 - 0.6 - 1.1 - 0.9 - 1.1	S 1.4 1.7 1.6 1.8 1.3 1.8 1.8	0.8 - A - 0.2 - 0.9 - 0.4 0 - 0.8 - 1.2 1.2 0.8 - 0.5 - 1.2
Average Minimum Maximum	1.6	0.27	2.06 1.3 2.5	0.32	1.91 2.8 2.3	0.64	1.58 1.3 2.1	0.32

Screen # 🕡	Scree Scre	en Diamet een Expos	pth (in.) ter (in.) sed (in.) ged (in.)	Po	Date: _ ersonnel: _	6-1- CSA) E	200 200	
		_ 6 -	<u></u>			<u>6</u> -	2	
Time Start Time End	150		150			2 f 32	9 2	2 f 32
Depth Vector 1 2 3 4 5 6 7 8	0 S 1.2 1.3 1.3 1.2 1.0 1.2 1.2 1.0	A 9.1 6.2 6.2 0.2 0.1 0.1 0.1 0.1	S 1, 5 1, 5 1, 4 1, 6 1, 6 1, 5	0.8 A 0.6 0.5 0.9 0.9 0.9 0.7	S .' .3 .2 . .3 .3 .2	0.8a - A - 0. \$ - 0. \$ - 0. 4 - 0. 3 - 0. 2 - 0. 9 - 0. 9 - 0. 9 - 0. 9	S 0.9 1.0 1.1 1.0 0.9 1.0	0.8 - A - c. 6 - 0. 7 - 0. 6 - 0. 9 - 0. 3 - 0. 3
10 Average Minimum	1.20	0.14	1.4	0.66	1.1	0.41	0.9	0.45
Maxi mum	1. 3	0.2	1.6	1 3	1.4	0.2	0.9	0.9

Notes:

- Screen u it turning and plugget

7.	Total Forebay Depth (in.) Screen Diameter (in.) 14 f Screen Exposed (in.) 3 (Screen Submerged (in.) 3 2						Pei	Date: _ rsonnel: _	6-1- C5A	- 89 225
Time Start	1452		I	1452			91	9		919
Time End	I /45			145	6		9:	22		922
Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z Z	<u> </u>		,			•				<u> </u>
Depth	i (). 2			0.8		. ().8a		0 .8
Vector	S	A		S	A		S	- A	S	- A
1	1.5	0.3		1.5	-0.4		1.7	-1.2	I. 6	– 1.3
2	1.5	0.2		1.9	1.7		2 2	-0.9	1.9	-0.2
3	1.6	0.3		1.0	0.9		1,6	-0.5	1.4	-0,8
4	1.7	0,4		1.8	0. 5		1.8	- 0, <u>s</u>	, 4	-0.4
5	- 1. S	0.2		15	1-1	ŀ	1.7	-0.6	1,7	-0.5
6	1 6	I 0.3		1.7	-0.4		2.0	-09	1.7	-0.2
7	-1.4 I	a.7		1.0	-2.2		1,	-1.0	1.2	-0.6
8	1.6	0.3		<i>I.</i> (<u></u>	- 6. 3		1.8	0	1.5	0.1
9	1 5	0.2		1.2	- 1.1		2.0	-0.7	1.4	0.4
10	1.6	0.3		14	0.3		1.9	-0,5	1,3	-0.6
Average	1.55	0.28		1.55	0.02	Į	1.85	0.68	1.53	
Mi ni mum	14	9 2		10	-2.2		1.6	0.0	1.3	-0.4
Maxi mum	1.7	4.4		1. 9	1.7		2.2	1.2	1.9	1.0

Screen #8	Total Forebay l Screen Dia Screen Exj Screen Subm	Date: _ Personnel: _	6-1- F9	
	<u>_</u> &	- (<u>6 -</u>	<u>Z</u>
Time Start	I 1314	1314	911	911
Time End	1317	1317	914	914
Depth	0. 2	0.8	0.8a	
Vector	S A	SIA	S - A	8.0 S I - A
1	1.7 a 4	1 0 0 2	1.3 -0.9	S - A 1. 7 1.3
2	1.7 0.3	2.5 1.2	1.6 -0.6	13 -01
3	1.7 0.2	2.1 1.9	1.1 -0.5	1.3 -0.3
4	1,7 0.4	1.8 0.9	1.8 -0.4	1.5 -0.8
5	1,8 0.4	1.8 0.1	1.7 -0.5	1.5 0.9
6	1.7 6.2	2.3 2.9	1,1 0	1.4 -0.4
7	1,600	1.4 1.7	1.9, -0.9	1.6 -0.2
8 9	1,7 0.3	1.4 -0.7	1.9 - 6.7	1.4 - 6.8
10	1,6 0.3	1.3 -0.4	1,3 -6.7	1.3 0.1
10	1 1/8 0/3	1,6 0.3	1.4 -0.8	1,6 -0.6
Average	1.70 0.32	1.84 0.91	1.51 2.50	1.46 0.17
Mi ni mum	1.6 0.2	1.3 -0.7	1.1 0.0	1.3 -1.3
Maxi mum	1, E 9 Y	2.5 2.9	1.9 0.9	1.7 0.9

Total Forebay Depth (in.) 140
Screen Diameter (in.) 66
Screen Exposed (in.) 36
Screen Submerged (in.) 132

Date: 6-1-69
Personnel: 254/200

ime Start	1 130	3	130		85		85	
Time End	13	07	130	7	90	0	900	<u> </u>
Depth		0.2		0.8		0.8a		0.8
Vector	S	A	S	Α	S	~ A	S	~ A
1	1.0	0.4	1.7	0.8	2.0	-1.0	1.4	0,5
2	1.6	0.3	1.7	2.8	1.2	-0.7	0.9	0,6
3	1.6	0.2	2.0	-1.4	1.1	-0.5	1.0	-0,0
4	1.7	0.4	2.6	2.1	2/1	-0.6	1,2	- o.y
5	1.7	0.3	1.4	-0.7	1.5	-0.9	1.5	1.3
6	1.6	0.3	1.4	-0.7	1,8	-1,0	J. J	-1.6
7	1. C	0.3	1.4	0.9	1.7	-06	1.1	- 0.
8	1,7	0.2	2.7	3.1	1.9	-1.5	1.1	-0.
9	1.6	0.3	2.1	1,4	1, 1	-0,6	1,0	- 1.4
10	1.6	ο.	2.0	2. 4	1.7	-0.9	1.0	-0.4
				 				
Average	1-62	0,30	1,90	1.07	1.61	7,23	4.75	₽. €
Mi ni mum	1.6	0.2	1. 4	-1.4	1.1	0.5	0 9	-1.3
Maxi mum	1.7	04	2.7-	3.1	2.1	1.5	15	1.0

Screen # (0	Total Foreba Screen I Screen Screen Su	Personnel:	6-1-89 CSA1 000	
		<u>6 · 1</u>		<u>· 2</u>
Time Start	I 1254	1254	848	848
Time End	1257	1257	851	851
Depth Vector 1 2 3 4 5 6 7 8 9 10	1. C 0 1. 7 0 1. 8 0 1. 9 0 1. 9 0 1. 9 0 1. 7 0 1. 7 0	.2 1.7 1.8	0.8a S - A 1.5 - 0.1 1.7 - 0.4 2.3 - 0.3 1.2 - 0.3 1.7 - 0.8 2.2 - 0.9 1.8 - 0.3 1.5 - 0.7 2.5 - 1.6	0.8 S - A 1.2 -0 7 1.0 -1.3 1.0 -1.4 1.2 -1.2 1.4 0.5 1.1 -0.2 1.3 -0.4 1.2 -1.3
Average Mi ni mum		32 1.53 0.11 2 0.3 -2.4	1.72 0.60	1.16 57-1
Maxi mum		9 2.1 1.8	2.5 1.6	1.3 -0.5

Notes:

center of screens perpendicular to dis corner of net pen & z

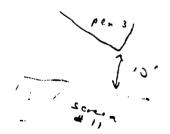


Total Forebay Depth (in.) 140
Screen Diameter (in.) 168
Screen Exposed (in.) 36 b-1- 89 Date: Personnel: CSA DOO Screen Subnerged (in.) 132 6-1 12 31 1231 Time Start 840 340 Time End 1235 1235 £47 843 0.8a 0.2 0.8 0.8 Depth Vector A A - A 1.3 0.1 0.4 6 ا -0.2 1.0 -0. -04 1.4 0.1 C Y 0.0 0.9 -0.9 -07 1.2 1. 5 0 -0.2 2.0 4 0 - 0.3 1. 3 0.1 0 . 1 1.3 0 1.7 0.5 1.4 - 0 4 Ċ 6 1,3 0 1 0.4 -02 0,9 - C./ 8 1.3 0.2 1.6 0.2 1.3 1.1 9 1.3 1.3 -0.4 0.1 1.5 0.4 13 1.6 — ৩. ২ 10 1.2 1.5 0.9 7 0 0.1 1.32 0.1 1.60 0.29 0.18 Average 0. Mi ni mum 0 -0.1 1.2 2. ø 1. 5 1.1 Maxi mum 1.4 0.2

Notes:

6/1.2 screen not turning and plugge I.

alower corner of pen # 3 (downstream pen) is just downstream of the Screen centerline, 1,0' from screen force



Screen # 12	Scre Scr	orebay De een Diane reen Expo en Subner	Date: _ Personnel: _	6- I-P? Cra/ado	
		<u> </u>	<u>I</u>	_8_	- 2
Time Start	1219		1219	832	f 32
Time End	12 2 3	3	1223	835	535
Depth	1 (0.2	0.8	^ ^ -	
Vector	S	Ĭ A	S I A	0.8a S - A	0.8
1	1.6	0 4	2,8). 4	1.3 -0.2	S - A
2	1.7	0.4	1.7 1.0	1.3 -02	1, 4 0, 4 0, 4 0, 4
3	1.60	0 4	1.4 -1.2	14 -0.1	1,2 0.1
4	1:50	0.4.	0.9 - 0.3	2.1 -07	1.2 0.4
5	17	0.4	1.8 -1.5	21 -0.7	12 - 0.2
6	1. 5	0.3	2.2 1.4	2.0 -0.5	1.0 -0.2
	1.5	0.3	1.8 1.4	1.9 -0.6	1. 3 - 0 Z
8	1.5	0.3	2.2 -3.6	1.6 - 0.8	1.1 -0.4
9	1.6	0.4	1.0 4.3	2.1 -0.5	1. 3 -0.2.
10	1, 6	0.3	2.8 3.2	1.6 -0.2	1.0 -0.4
Average	1.60	0.36	1.86 -0.25	1.74 2.47	
M ni mum	15	0.3	0.9 -4.3	1.3 0.1	1.16 0. /
Maxi mum	1.7	° 3	2.5 3.2	2 1 0.9	14 0.6

Notes:

notes:
6-f extreme variability in approach volucity at 0. A 2

Total Forebay Depth (in.) 140 Screen Diameter (in.) 158 Screen Exposed (in.) 36 Screen \$\frac{1}{5}					Pe	Date: _ rsonnel: _	C-I-S?	
		6	- I			b - 2	2	
Time Start	1209		1209		822		822	
Time End	121	3	1213		8 Z 7		527	
Depth Vector 1 2 3 4 5 6 7 8 9 10	S 1.2 0.9 0.9 0.9 1.1 0.5 1.0 0.9	0.2 0.4 0.7 0.7 0.3 0.3 0.7 0.7	S 1. 6 1. 7 2.0 1. 6 1. 7 1. 9 1. 9	0.8 A D.1 D.4 O.5 O.7 O.7 O.7 O.6 O.3 -0.7 D.9	S 1.8 1.5 1.7 1.6 1.8 1.9 1.9 1.7 1.9	0.8a - A - 0.8 - 0.5 - 0.5 - 0.5 - 0.7 - 0.7 - 0.6 - 0.6	S 1.2 1.1 1.1 1.2 1.2 1.4 1.1 1.1 1.2	0.8 - A - D.6 - O.4 - O.4 - O.3 4 O.5 - O.7 - 4.3 + O.2 - O.4
Average Minimum Maximum	94 0.8	0.3	1.67	0.78	1.7/	0.3	1.16	0.40

Screen <u># 14</u>	Total Forebay Depth (in.) Screen Diameter (in.) Screen Exposed (in.) 36 Screen Subnerged (in.) 132						Personnel: CSA/DOD			
		<u>. 6</u>	- 1					<u>6 -</u>	2	
Time Start	1200			1200		ſ	813		813	
Time End	1203			1203		[816		816	
Depth	1 (0. 2	0.8		1.8	r	.0.8a		0.8	
Vector	S	A		S	A	ĺ	S -	5 - A	S	1 - A
1	1.2	0.3	1	1.2	0.8	ı	1.4	-0.3	0.8	-04
2	1.2	0. 3		1. 3	0, 5	Ī	1.5	-0. 6	0 9	-0.3
3	1.2	0.3		1.3	0.6		1.2 -	-04	0.9	0.1
4	1.0	0.4		1. 3	0.2		1.3	-0.5	0.9	-0.2
5	1.1	0.3		1. 3	0.6	[1.2	-0.4	0.9	-0.8
6	1.1	0.3		1. S	9.0		1.1	-0.4	0.6	-0.6
7	1.0	9.4		1,4	0.9		1. 3	-0.6	0.8	-0.5
8	0.9	0.3		1.3	0		1.3	-0.4	0.9	-0.5
9	1.0	0 - 3	1	1.6	6.9	1	1.6	-0.7	1.1	-0.3
10	1.0	0.3	Ш	1.7	1.3	. [1,0	-0.4	08	-0.5
			1.							
Average	1.07	0.32		1.34	0.66		1.29	0.47	0.88	2.45
Mi ni mum	0.1	0 . 3		1, 2	O		1.0	0.3	0.8	-0./
Maxi mum	1.2	٧. ٥	ll	1.7	1.3		1.6	0.7	1.1	0.8
Notos										

Notes:

Some vector or #15

Screen # <u>\</u> S	Total Forebay De Screen Dian Screen Exp Screen Subne	Date: 6-1-59 Personnel: CSA/DDB					
Time Start	1142	[142	8=3	803			
Tine End	1145	1145	806	×06			
Depth Vector 1 2 3 4 5 6 7 8 9 10	0.2 S A 0.9 0.4 0.7 0.4 0.8 0.9 0.8 0.3 0.8 0.3 0.8 0.3 1.0 0.4 0.7 0.5 0.8 0.3 1.0 0.4 0.8 0.3 1.0 0.5	0.8 S	0.8a S -A 1.1 -0.8 1.2 -0.7 1.2 -0.8 1.4 -0.6 1.2 -0.7 1.1 -0.8 1.2 -0.6 1.1 -0.7 1.1 -0.7 1.2 -0.7	0.8 S -A 0.4 -0.8 0.7 -0.6 0.6 -0.7 0.7 -0.8 0.1 -0.8 0.5 -0.7 0.7 -0.8 0.7 -0.8 0.7 -0.8 0.8 -0.9 0.7 -0.8 0.8 -0.9 0.7 -1.0			
Notes: +x = approach sweep, for all 15 screens							
6/2/89 0.8 Sweep = +x } unit 824 0.8 Approach = -y } unit 824							
0.8a Surep = +4 Unit 1020 0.8a Approch = -x 3							

Total Forebay Depth (in.) /40
Screen Diameter (in.) /68
Screen Exposed (in.) 36
Screen Submerged (in.) 132

Time Start	151		15	10				
Time End	<i>15</i> I	4	15,	Ч.		***		
Depth		0.2		0.8		0.8a		0.8
Vector	S	Α	S	A	S	A	1	S A
1	1.6	0 1	1.5	-0.7			1	
2	1,5	01	1.5	-0.3			1	
3	1.5	0.3	1.50	-0.2			1 —	
4	1.4	-0.2	1.6-	-0.3				
5	1.5	0.7	1.6	-0.5			1	
6	16	-0.4	1.5	-0.5			1	
7	1.6	-0.3	1.5	- o. ¿s				
8	1.6	-0.1	1.6	-0.3			1	
9	ا، ل	0./	1.5	-04			1 [
10	1.7	-0.3	1.7	0.2			\mathbf{L}^{-}	
Average	1,57	-0.06	1.56	a38				
Mi ni mum	,	-a4	1.5	- U · F				
Maximum	1.3	0.2	1.	0.2				

Total Forebay Depth (in.) / 40

Screen Diameter (in. 1166

Screen Exposed (in.) 34

Screen \$\frac{\psi}{\screen}\$ Screen Submerged (in.) 172

Time Start	124	3	124	' 3		_				
Time End	1 12 4	16	12	46						
Depth	T	0.2		0.8	-).8a	+ -		0.8
Vector	S	A	S	A		S	A		S	A
1	1.7	-0.1	1.5	-0.6						
2	1.8	-0.2	1.7	0.1						
3	1.7	0	1.4	0.4				┚┕		
4	1,9	-0.1	1.4	-0.2				┛┕		
5	1.7	٥	1.9	-0.8				<u> </u>		
6	2.0	-0.2	1.60	-0.4	<u> </u>			┧┞		
7	1.9	-0.1	1.5	-1.4				⇃⇂		
8	1.7	0	1,5	-0.4				╛┕		
9	1.8	0.2	1.4	0.3			ļ	╛┕		
10	1.7	-0.1	1.6	0.1			l	41		
		T 4 ./	1 20		L			4		T
Average	1.79	-0.06	1.57		 			┥┷		
Mi ni mum	1.7	-0.2	1,4	- 1.4				44-		ļ
Maxi mum	2 0	0.2	1.9	9.4				┵		

Notes:

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Screen # <u>By<i>P</i>as</u>	Total Forebay Do Screen Diam Screen Expo Screen Submen	epth (in.) /40 '' eter (in.) 168 '' osed (in.) 36 " rged (in.) /32 *	Date:	6/1/89 25a1000 9' Forebay Elevation
Time Start	1124	1124		
Time End	1128	1128		
Depth	0.2	0.8	0.8a	0.8
Vector	S A	S A	SA	SA
1	1.6 -0.2	1.6 0		
2	1.6 -0.1	1.5 -1.0		
3	1.6 -0.1	1.2 -1.1		
5	1.7 0	1.6 0.4		
6	1.7 0	1.3 -0.7		
7	1.8 -0.1	1,5 -04		
8	1.80 1	1.5 0.8		
9	1.8 -01	1.1 -1.4		
10	1.6 -0.1	1.4 -0.2		
Average	1.68 -0.1	1.44 -0.33		
<u>Mi ni mum</u>	1.b -0.2	1.1 -1.4		
Maxi mum	1.8	1.7 0.8		
Notes: 0,2 2	= Unit 818.	0.8 2 = Unit 10 &	Used for a Meesurements	U 0.2 10.82, including cham screens.
44	3 Hoptoacri.			100

Screen #	Screen Diar Screen Ext	Depth (in.) 140 meter (in.) 168 mosed (in.) 36 merged (in.) 132	Personnel: -	6 15/37 6/6/89 Hong, 200r
Time Start Time End	I 1014 I 1017	1014	1752	1752
Depth Vector 1 2 3 4 5 6 7 8 9	0.2 S A 1.5 0.4 1.1 0.2 1.5 0.9 1.4 0.5 1.6 0.6 1.1 0.2 1.1 0.2 1.1 0.2 1.1 0.2 1.1 0.2	0.8 S A 0.0 -1.7 0.6 -1.4 0.3 1.9 0.5 0.4 2.4 2.1 2.2 1.6 2.0 -0.8 1.2 1.5 0.5 0.8 0.6 -0.6	0.8a S -A 0.9 -0.5 1.6 -0.9 1.0 -0.4 1.5 -0.8 1.7 -0.8 1.3 -0.6 0.6 -0.5 1.7 -0.8 1.0 -0.7 1.0 -0.7	0.8 S -A 1.2 -0.2 1.1 -0.6 0.2 -0.8 1.4 -1.2 0.7 -1.0 1.4 -0.9 0.7 -0.4 0.7 -0.6 1.1 -0.8
Average M ni num Maxi num	1.29 0.35 1.0 0.0 1.6 0.6	1.0 3 6.38 0.0 -1.7 2.4 2.1	1.30 0.63 0.6 0.4 1.7 0.8	0.99 7.72 0.4 0.2

Notes:

india programa in the second

Screen <u># 2</u>	Screen Dian Screen Ex	Depth (in.) 140 ueter (in.) 148 uposed (in.) 36 erged (in.) /32	. Date: Personnel:-	6/5/89 6/6/89 Hanf Abor
Time Start Time End	1007 1010	1007	1742	789
Depth Vector 1 2 3 4 5 6 7 8 9	0.2 S A 1.6 0.3 1.8 0.3 1.6 0.3 1.6 0.4 1.4 0.4 1.4 0.3 1.5 0.3 1.7 0.4 1.8 0.3	0.8 S A 1.4 0.0 2.0 1.0 1.3 -0.1 1.6 0.5 1.5 0.5 1.4 0.3 1.6 0.3 1.6 0.4	0.8a S A 1.3 -0.6 1.6 -0.5 1.7 -0.5 2.7 -0.5 1.9 -0.6 2.0 -0.6 1.9 -0.6 2.0 -0.6 1.8 -0.5 1.8 -0.5	0.8 S A 1.5 -0.4 1.5 -0.4 1.6 -0.4 1.7 -0.6 1.7 -0.5 1.4 -0.4 1.5 -0.3 1.4 -0.5
Average Minimum Maximum	1.60 0.33 1.4 0.3 1.8 0.4	1.5 4 0.36 1.3 -0.1 2.0 0.6	1,86 0,56 1.6 0.5 2.1 0.4	1.53 0.47 1.4 0.3 1.7 0.7

Screen # 3	Total Forebay De Screen Diane Screen Expo Screen Subner	ter (in.) /68 sed (in.) 36	Date: _ Personnel : _	6/5/89 6/6/89 Hart for
	J- 6/6/	24 	6/5	139 -
Time Start Time End	I 0959	0959	/733 /737	1733
Depth Vector 1 2 3 4 5 6 7 8 9	0.2 S A 2.0 0,3 7.3 0.2 1.8 0.3 3.6 2.5 7.9 0.2 1.7 0.2 7.8 0.0 2.9 7.9 7.9 7.0 3.2 2.5	0.8 S A 1.8 0.2 1.8 0.5 1.3 0.3 1.8 0.2 1.7 0.3 1.8 0.5 0.7 -0.2 1.0 -0.4 1.3 0.4 0.6 -0.6	0.88 S -A 0.3 -0.5 1.9 -0.4 2.4 -1.1 0.5 -0.4 2.4 -0.4 2.2 -0.5 -0.9 -0.2 1.4 -0.2 0,3 -0.2	0.8 S - A 2.4 - 0.9 1.6 - 0.4 2.6 - 2.0 1.8 - 2.0 0.9 - 0.6 0.9 0.1 0.7 - 0.2 1.9 - 0.7 2.5 - 0.9 1.9 - 0.8
Average Minimum Maximum	2 2 6 0.41 1.8 8.0 3.6 2.5	1.76 0.12 0.6 -0.6 1.8 0.5	0.24 2.35 -3.2 0.2 2.4 1.1	1.704

Screen <u>#c4e</u>	Total Forebay De Screen Diane Screen Expos en Submerg	Date: _ Personnel:_	6/5/39 6/6/29 Honf , Mor	
Time Start	1 0752	9 0952	1722	69 ————————————————————————————————————
Time End	0955	0955	1725	1725
Depth Vector 1 2 3 4 5 6 7 8 9 10	0.2 S A 1.7 0.3 2.0 0.3 1.9 0.3 2.1 0.3 1.9 0.3 2.0 0.3 2.0 0.3 2.0 0.3 1.9 0.3 1.9 0.3 1.9 0.3	0.8 S A 1.5 O.2 1.6 O.3 1.7 O.3 1.6 O.3 1.7 O.3 1.7 O.2 1.5 O.4 1.7 O.2	0.8a S A 1.9 -0.6 1.9 -0.6 2.0 -0.8 2.1 -0.7 2.1 -0.6 2.0 -0.7 2.0 -0.8 1.9 -0.6 1.8 -0.6 2.0 -0.7	0.8 S A 1.6 -0.4 1.5 -0.5 1.7 -0.5 1.7 -0.6 1.6 -0.7 1.5 -0.6 1.6 -0.7 1.6 -0.7 1.6 -0.7
Average Mi ni mum Maxi mum	1.9.3 0.30 7 0.3 2.1 0.3	1.62 0.27 1.5 0.1 1.7 0.4	1.97 0.67 1.8 0.6 2.1 0.8	1.62 0.62 1.5 0.4 1.7 1.0

Screen <u># 5</u>		Date: _ Personnel: _	6/5/84 6/6/24 an Ar	
	r-6/6/8	,	T-6/5/3	9 —
Time Start	0945	0945	1711	1711
Time End	I 0948	0948	1714	1714
Depth Vector 1 2 3 4 5 6 7 8 9 10	0.2 S A 2.0 0,3 2.0 0.3 2.1 0.4 2.0 0.3 2.1 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.4 2.0 0.3 2.1 0.3	0.8 S A 1.7 0.3 1.7 0.4 1.8 0.4 1.7 0.2 1.7 0.3 1.8 0.3 1.7 0.2 1.7 0.2 1.7 0.2 1.7 0.3 1.8 0.3	0.8a S -A 2.2 -0.6 2.1 -0.3 2.1 -0.7 2.2 -0.6 2.3 -0.6 2.0 -0.7 2.0 -0.6 2.0 -0.8	0.8 S -A 1.8 -0.6 1.7 -0.3 1.9 -0.6 1.3 -0.7 1.9 -0.5 1.9 -0.5 1.9 -0.6 1.7 -0.4 1.7 -0.6 1.6 -0.6
Average Mi ni num Maxi num	2.03 0. 2.0 0.3 2./ 0.Y	1.71 0.29 1.6 0.2 1.8 0.4	2.12 0.66 2.0 0.6 2.3 0.8	1.78 2.56 1.6 0.3 1.9 0.7

Screen <u>#</u> 6	Screen Diam Screen Expo	Depth (in.) 140 eter (in.) 168 sed (in.) 36 erged (in.) 132	Date: Personnel:	6/5/89 6/6/39 Hant Amor
Time Start	- 6/6 /89 — I 0939	0939	1703	
Time End	1 0941	0941	1706	1703
Depth Vector 1 2 3 4 5 6 7 8 9 10	0.2 S A 1.6 0.2 1.3 0.2 1.4 0.2 1.2 0.1 1.4 0.2 1.4 0.1 1.4 0.1 1.4 0.1 1.4 0.1 1.4 0.1 1.4 0.1	0.8 S A 0.9 0.3 0.7 0.2 1.1 0.4 0.8 0.2 0.9 0.3 0.9 0.5 1.1 0.3 0.9 0.3 0.9 0.3	0.8a S	0.8 S -A 1.0 -0.6 1.0 -0.6 1.1 -0.5 1.1 -0.6 1.1 -0.6 0.9 -0.6 0.9 -0.6 0.9 -0.6
Average Minimum Maximum	1.37 0.16 1.1 0.1 1.6 0.3	0.91 0.29 0.7 0.2	0.93 0.43	0.99 0.57 0.8 0.4

Screen <u># 7</u>	Screen E	Depth (in.) //6 meter (in.) /68 xposed (in.) 32 merged (in.) /32	Date: _ Personnel:_	6/5/89; 6/6 /39 Harf, Aber
	6/6,			/99
Time Start	I 0931	0931	1651	1651
Time End	0934	0934	1654	1654
Depth Vector 1 2 3 4 5 6 7 8 9	0.2 S A 1.8 0.3 1.9 0.3 1.9 0.3 1.8 0.4 2.0 0.4 1.9 0.4 2.0 0.4 1.9 0.2 1.9 0.3 1.8 0.3	1.7 0.5	0.8a S -A 1.7 -0.4 1.6 -0.3 1.6 -0.1 1.5 -0.2 1.5 -0.4 2.3 -0.4 2.0 -0.1 2.1 -0.4 1.7 -0.3 1.7 -0.2	0.8 S -A J.5 -0.9 J.5 -0.6 J.3 -0.7 J.4 -0.3 J.4 -0.5 J.5 -0.6 J.5 -0.7 J.5 -0.6 J.5 -0.7
Average Minimum	1.88 0.33		1.79 0.28	1.43 0.58 1.3 0.3
Maxi mum	2.0 0.4	1.8 0.8	2.3 0.4	1.5 0.9

Notes:

ALL READINGS SCIENTLY UNSTABLE, NEBOLE OSCILLATING (6/5/89)

Readings slightly unstable on 6/6/89 olas CLB.

Screen <u>#</u> 8	Total Forebay Depth (in.) / 40 Screen Diameter (in.) / 6 8 Screen Exposed (in.) 3 6 Screen Subnerged (in.) / 3 2—			6/5/87 6/6/93 : Hanf Foon
Time Start	1 0724	0924	1643	1643
Time End	I 0927	0927	1646	1646
Depth Vector 1 2 3 4 5 6 7 8 9	0.2 S A 1.6 -0.2 1.8 0.3 1.8 0.3 1.8 0.4 2.0 0.3 1.9 0.3 1.9 0.3 1.9 0.3 2.0 0.3 2.1 0.3	0.8 S A 1.6 0.3 1.4 0.2 1.5 0.3 1.5 0.2 1.5 0.3 1.7 0.4 1.7 0.3 1.5 0.4	0.8a S -A 1.8 -0.6 1.9 -0.8 1.9 -0.5 2.0 -0.7 1.9 -0.7 1.4 -0.6 1.9 -0.6 2.2 -0.6 2.0 -0.6	0.8 S -A 1.3 -0.6 1.5 -0.9 1.4 -0.5 1.5 -0.6 1.5 -0.6 1.4 -0.7 1.6 -0.7 1.5 -0.4
Average Minimum Maximum	1.88 0.26 1.6 -0.2 2.1 0.4	1.53 0.28 1.4 0.2 1.6 0.4	1.90 0.63 1.8 0.5 2.2 0.8	1.44 0.61 1.3 0.4 1.6 0.9

Notes:

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Screen \$ <u>tcFe</u>	Scre	en Diane een Expos b me r g	ter (in.) /40 ter (in.) /68 sed (in.) 36 ed (in.) /32		6/5/89 6/6/39 Hant, Abur
Time Start	090	4	0904	1636	1636
Time End	090		0907	1639	1639
Depth Vector 1 2 3 4 5 6 7 8 9 10	S 1.9 1.9 1.9 1.9 1.8 1.8 1.8 1.9	0.2 A 0.3 0.3 0.4 0.4 0.4 0.4 0.3 0.3 0.4 0.3	0.8 S A 1.6 0.4 1.4 0.5 1.5 0.4 1.5 0.4 1.5 0.3 1.5 0.3 1.6 0.3 1.6 0.3 1.6 0.3	0.8a S -A 2.0 -0.8 2.0 -0.7 2.0 -0.7 1.9 -0.9 1.8 -0.7 2.1 -0.8 1.9 -0.8 1.9 -0.8 1.9 -0.7 1.8 -0.7	0.8 S -A 1.5 -0.7 1.6 -0.5 1.6 -0.6 1.6 -0.8 1.4 -0.7 1.5 -0.7 1.6 -0.9 1.7 -0.7 1.5 -0.6
Average	1.86	0.34	1.52 0.36	1.94 0.74	1.53 2.64
Mi ni mum	1,8	0.3	1.4 0.3	1.8 0.6	1.4 0.5
Maxi mum	. 9	0,4	1.6 0.5	2.1 0.9	1.60 0.8

Screen <u># /O</u>	Screen Diane Screen Expo	Depth (in.) / 40 ter (in.) /68 sed (in.) 3 36 erged (in.) / 32	Date: Personnel:	6/5/89 6/6/59 Fort Aber
	6/6/	89	-6151	'89
Time Start	0857	0857	1626	1626
Time End	1 0900	0900	1630	1630
Depth	0.2	0.8	0.8a	0.8
Vector	S A	SA	S -A	S — A
1	1.9 0.3	1.3 0.1	1.4 -0.4	1.4 -0.5
2	1.8 0,3	1.4 0.4	1.8 -0.5	1.5 -0.6
3	2,0 0,3	1.4 0.2	1.8 -0.5	1.5 -0.5
44	1.9 0.3	1.4 0.3	1.8 -0.2	1.7 -0.6
5	1.9 0.3	1.5- 0.4	0.6 -0.8	1.4 -0.4
6	1.9 0.3	1.5 0.3	2,10.6	1.6 = 0.0
7	1.9 0.3	1.6 0.5	1.9 -0.4	1.7 -0.6
8	1.9 0.3	1.5 0.3	1.7 -0.4	1.5 -0.4
9	2.0 0.3	1.3 0.2	1.8 -0.3	1.4 -0.5
10	1.9 0.3	1.6 0.3	1.6 -0.2	1.5 -0.4
			r	
Average	/.9I 0.3	1.45 0.30	1.65 0.43	1.52 0.45
Mi ni mum	1.8 0.3	1.3 0.1	0.6 0.2	1.4 0.0
Maxi mum	2.0 0.3	1.6 0.5	2.1 0.8	1.7 0.6

Notes: Hur / / /

Screen <u># //</u>	Screen Diane Screen Expo	pth (in.) 140 ter (in.) 148 sed (in.)36 ged (in.) 132	Personnel:	. 6/5/89 6/3/39 Hanf Abor
	F-616189-		J-6/5/8	39
Time Start	I 0849	0849	16 18	16/8
Time End	0852	0852	1621	1621
Depth Vector 1 2 3 4 5 6 7 8 9	0.2 S A 1.2 0.0 1.3 0.1 1.3 0.1 1.4 0.0 1.5 0.1 1.5 0.1 1.5 0.1 1.7 0.0 1.2 0.0	0.8 S A 1.0 0.0 1.2 0.1 1.1 0.0 1.0 0.0 0.8 0.0 1.1 0.0 1.1 0.0 1.1 0.0 1.1 0.0	0.8a S A 1.3 -0.4 1.2 -0.3 1.2 -0.3 1.2 -0.3 1.2 -0.3 1.1 -0.2 1.1 -0.3 1.3 -0.3 1.3 -0.3	0.8 S A 1.0 -0.4 0.9 -0.4 1.0 -0.3 1.0 -0.3 1.0 -0.4 0.9 -0.4 0.9 -0.4 0.9 -0.4 1.0 -0.3 1.0 -0.3
Average Minimum Maximum	1. 33 0.06 1. 2 0.0 1.5 0.1	1.0 4 0.0/ 0.8 0.0 1.2 0./	1.21 0.30 1.1 0.2 1.3 0.4	0.94 0.36 0.8 0.3 1.0 0.4

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Screen # /Z	Screen D Screen Ext	epth (in.) 140 iameter (in.) 168 osed (in.) 36 erged (in.) 132	Date: Personnel: ⅓	6/5/89 6/3 /89 lanf, Aber
T2 C4		/89-		189-
Time Start Time End	I 0842 I 0845	0842	1609	1609
Depth Vector	0. 2 I S A	0.8 S A	0.8a S -A	0.8 S —A
2 3 4 5 6	1.6 0.3 1.6 0.2 1.6 0.3 1.8 0.3 1.7 0.3 1.6 0.3	1.3 0.2 1.2 0.3 1.3 0.2 1.2 0.3 1.3 0.2 1.2 0.2 1.2 0.2 1.3 0.3	1.5 -0.4 1.7 -0.6 1.7 -0.5 1.5 -0.6 1.7 -0.6 1.4 -0.6 1.7 -0.7	1.0 -0.5 1.2 -0.5 1.1 -0.5 1.2 -0.4 1.2 -0.4 1.1 -0.4 1-2 -0.5
8 9 10 Average	1.6 0.3 1.6 0.3 1.6 0.3	1.26 0.23	1.6 -0.6 1.5 -0.6 1.5 -0.5 1.58 0.57	1.0 -0.6 1.3 -0.6 1.2 -0.4 1.15 0.51
Mi ni mum Maxi mum	1.6 0.2	1.3 0.3	1.7 0.7	1.0 0.4

Screen <u># /3</u>	Total Forebay De Screen Diane Screen Expo Screen Submer	ter (in.)/6 8 sed (in.)3 6 ged (in.)/3 2		6/5/89 6/6/39 DER HANF 5/89		
[Time Start	0835	0835	1602	1602		
Time End	1 0838	0838	1606	1606		
Depth Vector 1 2 3 4 5 6 7 8 9 10	0.2 S A 1.5 0.2 1.5 0.4 1.7 0.4 1.6 0.3 1.5 0.3 1.4 0.3 1.5 0.3 1.5 0.3 1.5 0.3 1.5 0.3	0.8 \$ A 1.0 0.3 1.2 0.4 1.1 0.2 1.0 0.5 1.1 0.4 1.1 0.4 1.0 0.3	0.8a S - A 1.6 -0.7 1.5 -0.6 1.3 -0.6 1.2 -0.5 1.6 -0.7 1.6 -0.8 1.2 -0.5 1.3 -0.6	0.8 S -A 1.1 -0.5 1.0 -0.5 1.0 -0.6 0.9 -0.6 1.1 -0.8 1.2 -0.6 1.2 -0.7 1.1 -0.6 1.0 -0.7		
Average Mi ni mum Maxi mum	1.52 0.37 1.4 0.2 1.7 0.4	1.0 0.3 1.2 0.5	1.39 0.6/ 1.2 0.5 1.6 0.8	1.06 0.61		

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Screen # 14	Screen Diame	Depth (in.) /40 ter (in.) /68 sed (in.) 3 6 rged (in.) /32	Oate: _ Personnel :	6/5/89 6/6/89 Hanf Abor
	-6/6/8			189-
Time Start	I 0327	0827	1554	1554 1557
Time End	0830	0830	1557	1557
Depth	0.2	0.8	0.8a	0.8
Vector	s I A	S A	S -A	S –A
1	1.5 4 0.3	1.0 0.4	1,2 -0,5	0.9 -0.6
2	1.4. 0.3	0.8 0.2	1.3 -0.6	0.9 -0.5
3	1.5 0.4	1.0 0.3	1.3 -0.6	0.9 -0.6
4	1.4 0.3	1.1 0.4	1.4 0-0.6	1.1 -0.6
5	1.7 0.3	1.0 0.2	1.4 -0.6	1.1 -0.6
6	1.4 0.3	0.9 0.3	1.4 0.5	1.0 -0.7
7	/, 2 0.2	1.1 0.3	1.3 -0.6	0.9 -0.6
8	1.5 0.3	1.1 0.3	1.3 -0.6	1.0 -0.7
9	1.4 0,3	0.9 0.3	1.4 -0.6	0.9 -0.7
10	11.4 1 0,3	1.0 0.3	1.3 -0.6	1.0 -0.5
	1	1 4 20	122 0 50	[002] [04]
Average	1,44 0.31	0,99 0,30	1.33 0.58	0.97 0.61
M ni mum	1.2 0.3	0.8 0.2		
<u>Maxi mum</u>	1.7 0.4	1.1 0.4	1.4 0.6	1.1 0.7

: Screen #_ <i>15</i>	Scr Sc	een Dian roon Evr	epth (in.) meter (in. mosed (in. rged (in.)) 168) 36	Date: Personnel :	: 6/5 - 6/6/29
Time Start	081	4/0 8	08/3	7	1544	15/89
Time End	082	2	082	<u>-</u>	1547	J
Depth	<u> </u>	0. 2	1	0.8	0.8a	0.8
Vector	S	Α_	S	A	S -A	S -A
1	1,4	0,5	1.0	0.4	1.1 -0.7	0.7 -0.7
2	1.0	0.5	1.0	0.5	1.2 -0.6	0.3 -0.6
2	1 3	0.4	0.9	0.4	1.1 -0.7	0.7 -0.7
4	1.2	0.4	0.9	0.4	1.2 -0.6	0.3 -0.%
5	1.2	0.5	0.9	0.4	1.1 -0.7	0.8 -0.7
7	1.1	0.4	0.9	0.5	1.0 -0.7	0.7 -0.7
8	1-1	0.4	1.0	0.4	1.3 -0.7	0.7 -0.8
9	1.2	0.4	0.3	0,3	1.2 -0.8	0.7 -0.7
10	1.4	04	0.9	0.4	1.1 -0.7	0.8 -0.6
	,			- 110		
Average	1.20	0.43	0.9/	C.42	1.14 0.69	
Mi ni mum Mayi mum	1,0	0,4	0.	0,3	1.0 0.6	97 0.6
Maxi mum	1,	0.5	1.0	013	1.3 0.8	0.7 0.8
Notes:6/3/489	+ y = 50 - x = A	weep pproach	,	+×		Same for all Screens.
Last net	,			,		
6/6/89	0.2.	= lluit	1020	0,	8 = cenit 82	4 /
. ,	+ × = +y =	Sweep Approac	ch	+, +,	x = Sweep 1 = Approach	Same for all screens

Screen # Bipa	Total Forebay De Screen Diamet Screen Expos	pth (in.) //40" ter (in.) sed (in.) ged (in.)	. Date: _ Personnel:_	6/6/30 Byz CSA
Time Start	1033	1038		
Time End	1041	1041		
Depth Vector 1 2 3 4 5 6 7 8 9 10	0.2 S A 1.6 0.2 1.7 -0.2 1.7 -0.1 1.9 -0.3 1.7 -0.3 1.7 -0.3 1.9 -0.2 1.8 0.4 1.9 -0.3	0.8 S A /,3 -0.6 /,2 -0.2 /,3 -0.6 /,3 -0.5 /,4 -0.7 /,3 -0.6 /,2 -0.5 /,3 -0.6 /,2 -0.5 /,3 -0.6 /,2 -0.5	0.8a S A	0.8 S A
Average	1.76 -0.06	1.28 -0.51		
Minimum Maximum	1.6 -0.3	1.2 -0.7		
Notes: Meas	curemen to taken	with Base of	vertical prop	in support rod

Notes: Measurements taken with Base of vertical probe support rod at upstream stopleg slot in each bypass; Probes 18" upstream in center line of bypass slot.

Same location as measurements of 6/1/89 csa.

Screen #B, wass	Screen Diame	pth (in.) /40" ter (in.) sed (in.) ged (in.)	• Date: Personnel:	66/39 - CSA RW4-
Time Start	1053	105-3	ī	
Time End	1056	1056	-	_
			<u> </u>	
Depth	0,2	0.8	0.8a	0.8
Vector	SA	ŜA	SIA	\ S A
1	2.0 0.0	1.3 -0.2		\ <u>\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\</u>
2	2.1 0.1	1,2 -0,2		
3	2.0 -0.3	1.3 -0.7		
4	2.0 -0.1	1.1 -0.1		
5	2.1. 0.1	1.2 -0.3		
6	1.9 -0.2	1.3 -0.4		
7	1.8 -0.4	1.3 -0.3		
8	1.9 ±0.0	1.3 -0.5		
9	1.8 0.1	1.2 -0,2		
10	2.1 3 -0.2	1,30.4		
Amonosto	1 (2 0 1 0 00 1			
Average M ni mum	1.9 3 - 0.09	1.25 -0.29		
Maxi mum Maxi mum	1.8 -0.4 2.1 0.1	1.1 -05		
MAXIIIIM	2./ 0./	1.3 -0.1		
Notes:			\	

Screen # Bypess	Total Forebay Der Screen Diamet Screen Expos Screen Submer	ter (in.)	Date:_ Personnel: <u>-</u>	6/6/89 CSQ/EWH	•
Time Start Time End	1105	1/05			
Depth Vector 1 2 3 4 5 6 7 8 9 10	0.2 S A 1.8 -0.2 1.6 -0.3 2.0 -0.3 2.0 0.0 1.8 -0.1 1.6 0.0 1.7 -0.2 1.8 0.0 1.7 -0.2 1.8 -0.3 1.7 -0.2 1.7 -0.2 1.8 0.0 1.7 -0.2	0.8 S A 1,3 -0.5 1.1 -0.4 1,3 0.5 1,2 0.0 1,4 -0.5 1,2 -0.5 1,2 -0.5 1,1 -0.3 1,2 -0.2 1,0 -0.3	0.8a S A	0.8	
Bottom of Ramp	T=+Approximate = Approximate =	ter Wing ward. Wing ward. Cation) at 18"	h or outer wall		(ga vom)

are e

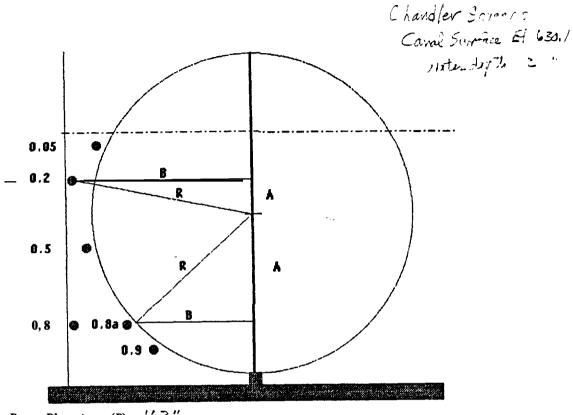
APPFNDIX C

CHANDLER SCREENS RAW DATA SHEETS

APPENDIX C

CHANDLER SCREENS RAW DATA SHEETS

This appendix contains the raw data sheets for flow measurements taken at the Chandler Screens on July 26 through 28. 1989. Page C. 2 shows the calculations made to position probes at the proper depths and the distance between the probe and the screen face at each depth. Raw data for measurements taken in front of the drum screens are presented on pages C. 3 through 8.25. Raw data for measurements taken at the entrance to the fish bypass pipes are shown on pages C. 26 through C. 28. A map showing measurement locations in the separation chamber is found on page C. 29, and raw data for measurements taken in the separation chamber are found on pages C. 30 through C. 34.



Drum Diameter (D): 162"
Radius (R): 27"
Exposed to Air (E): 54"
Submerged (Z): 188"

Measured dep Th = 1/2"; 4"+ seal reignt

Side A Side B 0.2 $Z : 2! \cdot 6$ 0.8 $Z : 96 \cdot 4$ 0.8 $Z : 95 \cdot 7$ 0.9 $Z : 97 \cdot 2$ 0.05 $Z : 5 \cdot 4$ 0.05 $Z : 5 \cdot 4$ 0.15 $Z : 5 \cdot$

Bistance From Vertical to Screen Face

0.2 Z: R-B=	0.18"
0.8 Z: R-B=	25.9"
0.8a Z: R-B=	
0.9 Z: R-B=	40.59
0.05 Z: R-B=	2,93
0.5 2: R-B=	4.63

Screen # /	en Diameter (in) Exposed (in) Submerged (in)	Forebay Ele Cana	vation 650/ I Flow //00 cfs	Date Pers	sonnel <u>1361 F.K.E</u>
Time Start /357 Time End Mode Unit 235 320	/357 /700 724 818				
3 0.5 0.1 0.1 0.1	U G L 0.8 S A Y A 0.2 0.1 0.1 0.2 0.4 0.1 0 0.2 0.4 0.1 0 0.2 0.7 0.1 0 0.2 0.3 0.1 0 0.2 0.3 0.1 0 0.2 1.3 0.1 0 0.2 1.3 0.1 0 0.2		U C L 0.9 S A V	U C L .05 S A V	U C L 0.5 S A V
Average 1// 0.02 7.06 6/0 Minimum 6.20 0.7 0.7 0.7 Maximum 0.6 0.1 0.7 0.7	0.2 0.1 -0.1 02				

Screen #		Scree	n Diameter Exposed Submerged	(in)	162 541 28	<u> </u>	Foreba	ay Ele Cana	vation I Flow	; /	. 3 · /00	<u>/</u> c /s				Date_ Perso	nnel _	. 6 2 20 20	179 516	<u> </u>
Time Start Time End Unit	1350		13 13 9211	50 54 818			1													
Location	U C	L	U Ø		7-	U 0.0		L	U	0.9			U	05	L		U	0.5	L	
Depth	0.2 S A V	T A	0.8 S A	-V A	┨┝╴		V	Т	s	<u> О. Э</u>	Γv		s	A	V		s	A	V	
Vector	S A V		0.5 0.1	0 0:	٦H		` `	 	╽├┷	<u> </u>	<u> </u>	\Box					П	\neg		
2	36 0 0		0.5 0.1		計一	\dashv		1												
3	0400		0.5 0.1			_		1												
4	07 0 1.	1 0.1	0.6 0	0.1 0.	ᅱᅡ	$\neg \vdash$														
5	0100		070	00	カロ															
6	0.5 0 0.		06 0	0 0.	7								<u> </u>							
7	27 0 0,		0.50	0 0.1	JE						L	<u> </u>					<u> </u>			\vdash
8	0.6 0 0.	2 0.1	0.6 0	0.10.	4 L			 _	 	<u> </u>			 							
9	0.7 0 0	10.1	0.5 0.1	0 0	4 L			_	 	ļ	<u> </u>	 	 	LI					 	
10	17 00.	1 0.1	0.50	0.10	」し				J L	L	<u> </u>	<u></u>	l L	L			L			
									1	1	τ	т			ì					
	060 0 -0								∤ ├──	 	├—	-	-			\vdash	-			\vdash
	10.4-0.1-0.		0.5 0	0 0.	4 F			+	╢	 	-	-	-			$\vdash \vdash \vdash$	-			\square
Maximum	10.700	0.1	0.7 0.1	0 0.	ᅬᆫ		l		J └──	l	<u> </u>	<u> </u>	l L			لــــا				

Screen # 3	en Diameler (in) <u>/6</u> Exposed (in) <u></u> Submerged (in) <u></u>	<u>/</u>	evatio <u>n á savi</u> al Flow <u>II co</u> e fs	Date Pers	<u> </u>
Time Start /343 Time End /348 Unit // // // // // // // // // // // // //	/343 /348 /24 8/8				
2 37 0 0.1 0.1 3 0.7 0.1 0.2 0. 4 0. 0 0.2 0.1 5 0.6 0 0.1 0.1 6 0.4 0 0.1 0.1	0.6 0.1 0 0.2 0.6 0.1 0 0.2 0.6 0.1 0 0.2 0.7 0 0 0.1 0.6 2 0 0.1 0.7 3.1 0.1 2.1	U C L 0.08a S A V	U C L 0.9 S A V	U C L .05 S A V	U C L 0.5 S A V
Average () (0,2) (2.15 (2.11) Minimum (0.4) (0 -0.3) (0.1 Maximum (0.9) (0.1) -0.1 (0.2)	0.6 0 -0.1 0.1				

Screen #	4	Scree	n Diameter Exposed Submerged	(in) <u>/6</u> (in) <u>~</u> d (i <u>n) /2</u>	2 1/ 2	Foi	rebay Ca	Elev	ation_ Flow_	<u> 1, 3</u>	100	· ·				Date_ Perso	/.	36, ' 36		- <u>e</u> .
Time Start	1336		133	3				_												
Time End	703 11		/3	400				_	ļ				<u> </u>				<u> </u>	—т		
Unit	703 11	٥.7	824	818	<u> </u>						L		L				L			
				•	U	С		_	U	C			- u	С	ī			C		\Box
Location	U ©	<u> </u>	U C			.08a	- _	ᅱ	Ť	0.9		\neg		.05				0.5		
Depth	0.2	$\frac{1}{2}$	0.8	VIA	s	A	VΙ	ᅱ	s	A			s	Α	٧		S	Α	V	
Vector	S A V	1/4	SA	V A 0.2	屵러	^+		寸		-:-								\neg		
1	0.7 0.1 0	2.2	0.7 0.1	0 0.2	-			-1			\vdash							\neg		
2	0.9 0.10.1	10.4			-			⊣				\vdash \vdash						$\neg \neg$		
3	2.9 0.1 0.	<u> 12:4</u>	0.7 0.1	0/ 0.4	\vdash	-		ᅱ	\vdash			Н	-							
4	0.9 0.10.	10.2	2.8 0.1	0 0.2	-			\dashv	-		\vdash	$\vdash \vdash$	_	-			П			
5	0.4 0.1 0	0.7	0.8 0.1		—	- 1		\dashv			 	Н		-		-				\Box
6	0.9 0.1 0.	10.7	2.4 2.1	0 0.1	-	-					 		\vdash	-		H			-	
7	0.8 0.1 0.1	0.2	0.70.1	0 0.2				\dashv			├		-	 		$\vdash \vdash \vdash$				\Box
88	0.9 0.1 0.	(0. 1	0.7 1.1	0 0.2	<u> </u>				├		 		-			\vdash				
9	0.9 0.1 0.		0.70.1	0 0.2	<u> </u>						-	1								_
10	0.9 0.10	0.1	0601	0 1.2	L				Ц	L	<u> </u>	!	L	L	L					
			1 21	. 01 0 1 2				\neg			τ	,		,						
	1.6 1.10 19	1 1 /2	0.74 11	-11 -1	-	 	-+	\dashv	 	 	 			 						
Minimum	0.7 0.1 -0.1	0,/	0.6 0.1	0.1 0.1	-	 		\dashv	-	 	\vdash									

Screen # <u>5</u>	en Diameter (in) /e Exposed (in) : Submerged (in) :	Forebay Ele Canal	vation 3 5 3 . 1 Flow 1/100 c ts	Date_ Perso	7/36/79 onnel <u>SM / F/6</u> (
Time Start /329 Time End /333 Unit // // // // // // // // // // // // //	1329 1333 8211 218				
Location U C L	U (2)	U C L	U C L	UCL	UCL
Location U C L Depth 0.2	0.8	0.08a	0.9	.05	0.5
Vector S A -V A	S A -V A	SAV	SAV	SAV	SAV
1 0.9 0.1 0.2 0.2	07 01 0 0.2 0.8 0.1 0.1 0.2 6.5 0.2 0 0.2 0.7 0.1 0 0.2				
2 11 0.1 0.2 0.2	0.8 0.1 0.1 0.2				
3 /.0 0.1 0.1 0.2	1,8 0,2 0 0,2				
1 4 0.9 0.1 0.1 0.2	127011010				
5 0.9 0.1 0.1 0.2	10.2101112 10.11				
1 6 13 9 1 8 / 1 8 1 8 / 1	1/0 71 4 /18 /18 0 01				
7 0.8 0.1 0.1 0.2	08 0.2 0 3.3				
8 0.8 0.1 0, 2 0.2	0.6 0.1 0.1 0.2				
9 2.8 0.1 0.1 0.2	27 01 0 0.2				
10 2.8 0.1 0.1 0.2	96 0.2 0 3.3 0.6 0.1 0.1 0.2 97 0.1 0 0.2 0.1 0 0.2				
		·			
Average OST OIC CIZ D.LO	1.15 0.1= 13-0.20				
Minimum 0.8 2.1 -0.2 0.72	0.7 0.1 -01 0.1				
Minimum 0.8 2.1 -0.2 0.2 Maximum /-/ 0.1 0.1 0.2	0.8 0.2 0 0.3				

Screen #	<u> </u>	, 2	Scre	Е	xpos	ed (n) /6 in) 5 n) /3.	7/	Fo	oreba	y Ele [,] Cana	vation Il Flow		/3=3 100	eFs				Date Perso	2 onnel	'25) Cl	181	E
Time Start		132	/	Г	132	2/																	
Time End		1323	5		/3	25														<u> </u>			
Unit	3:	2.3	1020	8	24	8	18			<u> </u>		L				L		L				L	
Location	Ū	C) [~~)					L	U	c			U	С	t		U	-c		_
Depth		0.2			0.8				.08a				0.9				.05				0.5		
Vector	s	A	-V A	S		_V	A	S	Α	٧		S	Α	٧		S	Α	٧		S	Α	٧	
1	09	0.1	0.1 0.2	0.8	0.1	0,1	0,2																
2	3.9	0,1	2.1 2.2	0.8	0,1	2,1	9.3									L							
3	21	2.1	1. 0.		0.1		0,2																
4	1.0	0,1	0.102	12.8	2.1	0	0,2					<u> </u>				<u> </u>	 		\vdash	\vdash		\square	<u> </u>
5	2,4	0.1	0. 1 0.2		21		2.2		<u> </u>			<u> </u>					<u> </u>					\square	
6	تمن		0.1 0.2	2.1	2.1	2.1	32					 		<u> </u>	L	 			Ш	\vdash		\vdash	<u> </u>
7	10	0.1	0.1 0.2	Cis	21	3./	0:2			<u> </u>		 	<u> </u>			 	<u> </u>	L				 	
8	1, 5	2.1	3.1 3.2	2.7	1 0.1	0					ļ	 	 -			<u> </u>	ļ	_		-		\vdash	<u> </u>
9	2,4	0.1	0.10.3	2.7	2./		0.2	ļ		!	ļ	 	!			ļ		<u> </u>		 		 	
10	0.9	9.1	0./2.2	<u>ن. ز</u>	0.1	0	2,2	<u></u>	L	<u></u>	<u> </u>	l	<u> </u>	L	i	L	L	<u> </u>		L	لــــا		
	2.8	0.1	0.11 CZE -0.2 0.2 -0.1 0.2	0.7	0.10	-0./	0.2																

Screen #	_ 7	_	Scree	Ex	cposed	r (in)/ <u>(</u> d (in) <u>5</u> l (in)/	-4		•	oreba	y Ele	evatio al Flo	<u>n 6</u> :	26 <u>30. </u> 100 '	- 6: 10	37 C1	S		Date Pers	7/2 onnel	26-2	27/	86 137
Time Sta			7/20		1314		26	<u></u>			7/27			17	7/27	<u> </u>	102		7/27		1020	2	1/27
Time End	/3.	8		<u></u>	1318	<u> </u>		<u> </u>	12	21			/	22	<u> </u>		16 2	3			102		
Unit				L				L		<u> </u>				<u> </u>		<u> </u>		<u> </u>		L_			
1			 1																				
Location		<u>c</u>	느니	r_U	<u>C</u>	<u> </u>		L U	С			LU			<u>L</u>	μ <u>υ</u>			L	U	<u>_</u>		<u>L</u>
Depth	0.				0.8				.08a	,			0.9				.05		, ,	<u></u>	0.5		
Vector	S A		A	S	Α		Щ	S	A	+∀_	A	<u>s</u>	<u> </u>	7	<u> </u>	S	I A	-∀	1	S	A	-٧	A
1		2 0.1		0.7			23	1.7	2.6	2.1	2.5	304	2.		2.4	1.0	0. /	0.1	0.2	0.9	0.2	0.1	0,3
2	1.0 0.	10.1	0.3	0.8	0.1		2:3	1.8	9. 8	0.1	2.5	2.6		-0.1					0,3	2.2	25	0.1	2,5
3		10	0.2	0.8		00	2.3	1.7		0.1	0.6	0.5	2.3		0,4		200	2.1	7 =	2. 1	2.1	2.1	7. 5
4	1.1 0.		0.3	97			2.2	1.9	0.8	and	0.6	0.5	02	-02	0,3	0.8	0.1	0.	0.5	0,0	20,5	2	0.2
5	0.9 0.	1 001			0.1		<u> 2.21</u>	1.8	0.6	0.1	0.5	0.6	0.7	-0,1	04	2.9	0.1	0,1	0,2	ثب وال	2.2	0	0,2
6	0,9 0,	2 0.1	2,3	0%	9.2	00	2.3	1.7	0.7	0,2	0.6	0.6	2.5	-0.1	0.3	1.0	0.1	0	2,2	1.9	0.1	0,1	2, 3
7	1.90	2 2.1	2.3	1.8	002	2.1 6	2.3	2.0	0,8	Cil	1.5	3%	2,3	0,7	1,3	0,9	11.	10	0,7	1.9	0,2	0.1	10.3
8	0.9 0.	2 0.1	0,3	0.8	0.2	00	2.3	1.8	0.7	0.1	0.6	0.7	0.3	0.1				10,2	3.5	3.7		0.1	0, =
9	1.0 0.			0.1	0.2	0 0	2,3		0.7	Del	0.7		0, 4		0.01	1.0	0.	10	3.5	217		0.1	
10		2 0,2		0.7			2.2	2.0	27	0.1	0.5	0.7	0,2	-a1	5.4	09	0.1	10.1	1):=	24		3.2	
																			•				
Average	0.97 01	8-009	0.29	73	016	0.01 0	.27	0.5%	0.70	00.2	61.55	0.	13		0.35	0,92	0.12	-0.09	9.74	2.78	0.17	-0.08	0.27
Minimum																		-					بعنت
Maximum																							

Notes:

, ´ Screen #	<u>8 </u>	n Diameter (in) // Exposed (in) // Submerged (in) //	Cana	7/16 7, ation <u>6 30 · 1 ~ 6 3</u> Il Fl <u>ow //0 0 ~ /o</u>	√2 7 p. 0 Date_ 37 c f ₃ Perso	7/23-21/64 onnel 24 1/6
Time Start Time End Unit	25 1/26 255	/251 1/2L /255	1210 7/27	1215 7/27	1312 7/27	13.5 7/27
Location Depth Vector 1 2 3 4 5 6 7 8 9	U C L 0.2 S A -V A 0.9 0.2 0.1 0.3 0.7 0.2 0.1 0.3 0.9 0.2 0.1 0.3 0.9 0.2 0.1 0.3 0.9 0.2 0.1 0.3 0.0 0.2 0.1 0.3 0.0 0.2 0.1 0.3 0.0 0.2 0.1 0.3 0.0 0.2 0.1 0.3 0.0 0.2 0.1 0.3 0.0 0.2 0.1 0.3	0.6 0.1 0 0.3 0.6 0.1 0 0.2 0.7 0.1 0 0.3 0.7 0.1 0 0.3 0.7 0.1 0 0.3 0.7 0.1 0 0.3 0.7 0.1 0 0.3	1.8 3.7 0.5 2.7	0,5 5,2-2 25	1.2. 0.2 0 3.3	0801 2 35
Average Minimum Maximum		0.75-0.02 0.28	0.94 0.75 0.0.162.76	0.4-0.1719. 5.10 4.29	0.77	2.18 ta 07 2.28

, Screen <u># 9</u>	een Diameter (in) / Exposed (in) / Submerged (in) /	<u>(₄ 2-</u>	7/26 evation <u>6 30.1 - 6 3</u> al Flow <u>110 0 - 73 3</u>	7/2 7 80. () Date 7 c √ S Perso	onnel <u>%a</u> Promi
Time Start /242 7/34 Time End /246 Unit	1242 7/21	1304 1/27		/005 7/27 /20°	1005 7/27
Location U G L Depth 0.2 Vector S A -V A 1 /.0 0.2 0.1 0.3 2 /.1 0.2 0.1 0.3 3 /.1 0.2 0.2 0.3 4 /.1 0.2 0.1 0.3 5 /.1 0.2 0.1 0.3 7 /.1 0.2 0.1 0.3 7 /.1 0.2 0.1 0.4 9 /.1 0.2 0.1 0.4 10 /.1 0.2 0.1 0.4	0.8 0.2 -0.1 0.4 0.8 0.3 -0.1 0.4 0.7 0.2 0 0.4 0.8 0.3 -0.1 0.4 0.8 0.2 -0.1 0.4 0.8 0.2 0 0.4	U C L 0.08a S A -V A 1.7 06 0.4 0.6 1.7 0.6 0.4 0.7 1.7 0.7 0.4 0.9 1.8 0.6 0.4 0.9 1.7 0.6 0.4 0.9 1.7 0.5 0.3 0.7 1.5 0.6 0.4 0.8 1.7 0.4 0.4 0.8 1.7 0.4 0.4 0.8	U C L 0.9 S A V)	U C L .05 S A -V A /// N J J J J // N J J J // N J J J // N J J J J // N J	U C L 0.5 S A -V / // 3/- 2/2 3/4 // 3 2 3/ 3/3 // 3 2 3/ 3/3 // 3 2 3/ 3/3 // 3 2 3/ 3/3 // 3 2 3/ 3/3 // 3 2 3/ 3/3 // 3 2 3/ 3/3 // 3 2 3/ 3/3 // 3 2 3/3 // 3
Average 1.10 0.24 01 0.35 Minimum Maximum	0.77 0.22 405 0.39	1.69 0.53 0.79		1.14 0.17 0.09 0.3	1.02- 220-214 037

Notes: Too Warter Sill to do \$1,09z (probes hung up/buried in mud). CAR 7/29

Screen # -	10)		Scree	Ex	posed	(in)_	16 54 10 ;		Fo	orebay	y Ele Cana	vation I Flow	6	30 /(00	. J e +s				Dale_ Perso	nnel _	1/26/ 243	794 1985
Time Start		123	1			123	4																
Time End		1239	6			/23 123	\check{q}											—					
Unit	2:	? 3	//)	28	7		ومهج	<u> </u>	L		<u></u>										<u> </u>		
																					- U		
Location	U		<u> </u>		U	C	<u>} </u>		U	С	<u> </u>		U	C			, U_	<u>C</u>		\dashv	r '	0.5	
Depth		0.2			<u></u>	0.8				.08a				0.9			-	.05			$\frac{1}{2}$		
Vector	S	A	7	A 0.3 0.3 0.3 0.3	s			A	S	Α	٧		S	Α		├ ─┤	S	<u> </u>			S	_A	<u> </u>
1	1.2	0.2	0.1	0.3	1.1	012	0.1	0.4				<u> </u>	 			Ь—Н						-	
2	1.1	0.1	0.1	03	1.1	0.2	0.1	0.3					<u> </u>				-	_			┝═╡		
3	1.2	a	0.2	0.3	1.0	0.2	0.1	0.3							ļ	\vdash	-						_
4	1.2	0.1	01	0.3	0.9	0.2					ļ		<u> </u>	ļ		\vdash	 				<u> </u>		
5	1.2	0.1	0.1	0.3	10	0.2			<u></u>				 							-		 -	
6	/./	0.2	0.1	0.3	1/./	0.2	0.1	0.4					 	<u> </u>	<u> </u>	 						<u> </u>	
7	1.1	0.2	0,2	0.3 0.3 0.3	1.1	0.2	0.1	2,4			<u> </u>		<u> </u>	 	L	11	<u> </u>				 		_
8	1.2	0. =	0.2	0.3	1./	02	0.1	0.3					l	ļ			<u></u>						
9	1.2	0.1	0.1	0.3	1.1	0.2	0.1	0.3	L_							ļ	<u> </u>					 -	
10	1.2	0.1	0.1	0.3	1.1	0.2	0.1	03	L				L	<u> </u>									لــــــــــــــــــــــــــــــــــــــ
											,	,							<u> </u>		rT		
Average	1.17	0.15	-0.13	1, 7, 2	1.16	0,20	0.10	5.44	<u> </u>				 		<u> </u>		<u></u>				\vdash		
Minimum									L						ļ						\vdash		
Maximum								- 1					L				L						

, [′] Screen #	Ι'	Scree	Ex	meter (in) posed (erged (ii	in) <i>S</i>	4	Fo	orebay C	Elevanal	vation Flow	6	30, 100	/ e 5				Date Pers	onnel	7/2 ex	6/8 1/f	9 16T
Time Start				227					\Box												
Time End Unit	/23	1020	14.	1231	110		—											-			
Oint	<u> </u>	770	٠,	29 8	· *	L				L			I	L		L		L			
Location	U 6	L	U	(<u>c</u>)		U	C	L		U	С	ī	_	υ	C	1		U	С		
Depth	0.2			0.8		0	.08a				0.9				.05				0.5		
Vector	S A	-V A	S	A -V		S	Α	٧		S	Α	٧		S	Α	٧		S	Α	V	
1	1.2 0.1	0.1 0.3	1.0	0.2 0	0.3																
2	1.2 0.2	0.1 0.3 0.1 0.3 0.1 0.3	1.0	0.2 0	0.3																
3	1.2 0.2	0.1 0.3	0.9	020	0.3																
4	1.3 0.2	01 0.3	1.0	02 0.1	0.3			[
5	7. 3145	ロルロマレ	17.61	$\alpha > 1 \wedge 1$	1 ~ >!																
6	15 15 5	احمانيما	1, , 1	00101	احما															\neg	
7	1.3 0.2	0.2 0.3	1.1	0.3 0	0.3																
8	1.2 0.2	0.2 0.3	1.1	1.2 0.1	0.3																
1 9	1.2 0.2	0.210.31	1001	0.21 0.1	10.31				\neg											$\neg \neg$	
10	1.2 a2	0.1 0.3	0.9	0.2 0.1	03				\neg											\neg	
1																,		<u></u>			
Minimage	1301	-0.2 0.35	£.10	0.21 -0.16	0,30															$\neg \tau$	
			2.9	0.2 -0.1	0.3				_]											\neg	
Maximum	1.3 0.2	·O./ 0.3	1.1	0.3 0	03														$\neg \uparrow$		

Screen #	12_	Scree	en Diameter Exposed Submerged	(in) / (in) (in)	<u>×</u> 7	Fo	rebay	Ele v Can	vation al Flo	<u>/</u> .	-3	<u>;</u> cfs				Date_ Perso	nnel _	100 CB,	'23 1881	
Time Start	122	21	122	/									L							
Time End	/22	5	/22	5									<u>L</u>				<u> </u>			
Unit	833	1020	122/ 122 121	نج اشتر					L				L				<u> </u>			
																				—.
Location	U C) L	UC) L	U	C			U		L		U				L <u>u</u>	C		
Depth	0.2		0.8		0	.08a			<u> </u>	0.9			<u> </u>	05			<u> </u>	0.5		
Vector	S A	-V A	S A	V A	S	Α	٧		S	Α	٧	$ldsymbol{\sqcup}$	S	Ą	٧	\Box	S	<u> </u>	V	
1	1.3 02	0.1 0.3	1.0 0.2	0.1 0.3							L	Ш	<u></u>			Ш				
2	1.3 0.2	0.1 0.3	1.10.2	0.1 0,3								Ш	└							
3	1.3 0.2	0.1 0.5	1.2 02	0 0.2																L
4	1.2 0.2	0.1 0.3	11.1 0.2 1	0.1 0.3								$ldsymbol{ldown}$	<u></u>							
5	13 0.2	0.1 0.3	1.1 0.2	01 0.4									<u></u>	L						
6	1.2 02	0.10.3	1.1 0.2	0 03																
7	1.3 0.2	0.1 0.3	1.0 0.2 1.0 0.1 1.1 0.2	0.1 0.3																
8	1.3 0.7	0.1 0.3	1.0 0.1	0 013								L								<u> </u>
9	1.3 0.2	0.1 0.3	1.1 2.2	00.3																Ĺ
10	1.2 0.1	0.10,3	1.1 0.2	9.1 0.3																L
	<u>. — </u>		<u> </u>																	
Average	1.27 0.19	O b 2.30	1.07 0.19	204 0.30									L_				Ш			
Minimur	1.2.0.1	-0.1 0.3	10 0.1	0.1 0.2												Ш				
Maximum	1,30,2	-0.10,3	1.2 0.2	0.1 0.4																

٠.

, ' Screen # <u>/ 3</u>	een Diameter (in)	Forebay EI Cana 7 7	evati <u>on i a /</u> al Flow // bo c fs	Date Pers	7/2 1/56 sonnel <u>26.75</u>
Time Start /2/5	1215 1219 734 818				
Time End (215	1218				
Unit 823 '020	X24 818				
Location U (C) L	U (C) L	UCL	11 0 1	ı - 	1
Depth 0.2	U (C) L	U C L 0.08a	U C L	U C L	U C L
Vector S A V A	S A V A	SAV	S A V	SIAIVI	0.5 S A V
1 1.1 0.1 0.1 0.3	1.0 02 0.1 0.4	╽ ╸╩╶╏╶ ┸╌┼	3 7 7	 3 7 V 	SAV
	1.1 0.3 0.1 0.3		 		Ĭ Ĭ
2 1.1 0.1 0.2 0.3 3 1.1 0.1 0.1 0.3	1.1 0.2 0 0.3		 	 	
4 1.0 0.1 0.1 0.3	1.1 0.2 0 0.3 1.0 0.2 0 0.3				
5 1.0 0.1 0.1 0.3	1111102 0103				
6 1.1 0.1 0.2 0.3	1.0 0.2 -01 02				
7 1.1 0.1 0.1 0.3	1.1 10.2 0.1 0.3 1.1 0.2 0.1 0.3				
8 1.0 0.1 0.1 0.3	1.1 0.2 0.1 0.3				
9 1.0 0.1 0.1 0.3	1.2 0.2 0.1 0.3				
10 0.9 0.1 0.1 0.	1.0 0.2 0 0.3				
1: (D 2) (D. 2)		·		· · · · · · · · · · · · · · · · · · ·	
Average 1.04 0.10 0.12 0.3	1.07 0.21 raph 0.50	<u> </u>			
Minimum 0.9 0.1 -0.2 0.3 Maximum 1, 0, 1 -0.1 0.3	17 07 01 012	 	 	 	
Maximum /, / 0, / 0, / 0, /	1.Z 0.3 C.1 0.4				

Screen #	_14so	creen Diameter (in) / 6 Exposed (<u>in) / 3</u> Submerged (in <u>) / 3</u>	-4	Forebay E Cai	levatio	<u>خ n</u>	30. 100	, ets				Date_ Perso	onnel	26	190 188	7
Time Start	1209	/209														
Time End	1212	1212			⅃ ᅵــــ				L_							
Unit	223 256	० ४३५ ४%	<u> </u>	<u> </u>	┙┕				<u> </u>				L			
Location	υ C L	U Ø L	U	C L	ں ٦				Ü	c				С		
Depth	U C L	0.8	0.08		┨厂	0.9				.05				0.5		
Vector	S A -V	A S A -V A	SA		s	Α	٧		S	Α	٧	П	S	Α	V	
1	1.2 0.2 0.1 0 1.2 0.2 0.1 0 1.2 0.2 0.1 0 1.3 0.2 0.1 0	1.3 1.0 0.1 0 0.3]											
2	1.2 0.2 0.1 0	3 0.9 0.2 0 03] [
3	1.2 0.2 0.1 0	.3 1.1 0.2 0 03]				<u> </u>							
4	1,3 0,2 0.1 0	1.3 1.0 0.2 0 0.3			⅃ ┣—				<u> </u>						\longrightarrow	
I 5	1/ スリムつしん // ム	しなしかりしょうしゅしりょ							 	_						ļ
6	1.3 0.2 0.10	13 1.1 0.2 0 0.3				\vdash			 			\vdash				
7	1.2 0.2 0.10	3 /· / 0.2 0 2.3 3 /· / 0.2 0 0.3 3 /· / 0.2 0 0.3 3 /· / 0.1 0 0.3 3 /· 0 0.2 0.1 0.3 3 /· 0 0.2 0 0.3		-					 				-			-
8	12 0.2 0.1 0	3 0.9 0.7 0 0.3		- -			-	├─┤		\vdash			\vdash			
9	1.30.20.10.	3 1.0 0.2 0.1 0.3		- -	┨├──	 		\vdash				$\vdash \vdash$	\vdash		-	-
10	11.2 0.2 0.70	1.000.210 10.3				11	<u> </u>		! L	L				1	1	
Minimum	1.24 20 0.0 0 1.2 0.2 -0.1 0 1.3 0.2 -0.1 0	.3 1.00 418 12.01 61.3 3 17.9 0.1 0.1 0.3 3 17.1 0.2 0 0.3														

Screen #/	en Diameter (in)// Exposed (in) 9	<u>2</u> Cana	7/26 7, evation <u>/6 35 . 1 - 6 3</u> Il Flow <u>// - / 0</u>	2 7 30.0 Date 37 cfs Pers	7/26-27/89 onnel <u>344/777</u>
Time Start /202 7/21 Time End /206 Unit	1202 7/26 1206	1150 7/2	1157 1/2	0957 767	10354 7/27
Location U C L	ис.	u c L	U C L	UCL	U (L
Depth 0.2 Vector S A -V A	0.8 S A ~V A	0.08a	0.9 S A ~ A	.05 S A -V /-2	0.5 S A V /r
1 1.0 0.2 0 0.4	S A -V A 0.9 0.2 0 0.3	1.10.4-010.6		13 82 3 5.14	S A -V /- 1 0.3 0.1 0.4
2 10 02 0.1 0.4	1.1 02 0 0.3	09 0.3 -011 0.5	0.7 0.4 -0.1 0.5	1,30.30.10.5	1.1 0: 0.1 3.4
3 1.0 0.2 0.1 04	1.0 0.2 0 0.4	1.1 0.3 -0.1 0.5	0.8 0.4 -0.1 0.5		1,2 3,2 0 93
4 1.0 0.1 0.1 0.4	1.0 0.2-0.1 0.4	1.0 0.4 -0.1 0.5	0.7 0.4 -0.1 0.5	33 01 20 23	1.1 0.2 0.1 0.4
5 1.0 0.2 0 0.4	0.8 0.2 0 0.3	1.1 0.3-0.1 0.4		1.3 0.2 2.1 0.3	1,2 0.2 0 0.4
6 1.0 0.1 0 0.4	1.0 0.2 -41 03	1.0 0.3 -0.10.5	0.7 0.4 -0.1 05		1.1 0.2 0.1 0.5
7 1.1 0.2 0.1 0.4	0.9 002 0 0.3	1.2040 0.5	1.0 0.4 .01 0.5	12 012 011 1.5	11 1. 01 019
8 1.1 0.2 0 0.4	1.0 0.2 0 0.3	1,1 0.41 -0.10.4	0.8 0.4 -0.1 2.5	42 32 31 7	1.1 1 5 2 314
9 1.1 0.1 0.1 0.9		1.2 0.4 0.13.5	7.5 0.5 0.10.5	. 5 7 7	10 7 3 3 3 3
10 0.9 0.1 0.1 0.4	1.0 0.3 0 0.4	1.1 0.30.10.4	2.8 0.4 .31 3.5	15 3.7 21 2.8	11 02 0 01
Average /.02 0.16 -00 0.46	0.99 0.21 6.02 0 32	1.020.250.09 2.49	077 0.24 0.16 0.50	1.27 0.20-0.08 0.31	1 12 D22 - DAV 0.34
Minimum	9.70	37 15-10	10,77 0,77 0,30	1.07 0.20 0.08 4.37	1.16 0.25 007 17.75
Maximum					

Forebay Elevation 630.1-630.0 Date 7/26-27/85

Canal Flow 1100 - 103 7c fs Personnel Cox 1015 Screen Diameter (in) / / Screen # Exposed (in) 54 Submerged (in) / 2 8 2049 13/3 7/24 7/26 1156 1156 Time Start 1200 Time End 1200 Unit С u С С Ū С U C Location 0.5 .05 0.9 0.08a 0.8 0.2 Depth S Α SAW A -V Vector -0.10:2 0.9 0.2 -0.3 0.30 0+ 10 1.14 0.27 0.06 0.44 1.06 0.24 0.04 0.39 Average 1.18 3.14 aps 6.40 0.91 0.17 6.33 0.32 1.19 0.44 0/3 0.58 Minimum Maximum

Large obstruction under Screen - No 0.97 mil 11 11 11 1 1/89

7/26 7/27

Forebay Elevation 630.1 - 633.0 Date 7/26-27/89

Canal Flow 1100 - 1037cf3 Personnel Cas / PBF

, Screen # 17____

Screen Diameter (in) 1/6 2 Exposed (in) 5-1 Submerged (in) 1/2 8

Time Start Time End Unit	1148 7	24	1148	7/26		1141	7/27	//	41		7/27		79 42	<u> </u>	3/27		142	7/27
Location Depth	U C L	Ų	C L		0.0	(C)	L	U	0.9	<u>)</u>		U	.05	L		U	C	L
Vector) s		A	s]	A -V	14-	s	A A	~V]	A	S		-v T	A	s	0.5 A	VA
1	1.2 0.4 0.1	.5 0.8	0.6 0	0.7	0,90	40.5		0.7	3.7	0	0.4	1.3	0.3	4.7	3.5	1.0		0.2 0.6
2	1.2 0.4 0.1	5 04	07 0.1	08	100	6 2.1	0.2	2.7	2.7	0	1.8	7.2	0.2	0.1	0.5	ج .و	1.1	1.1 0.5
3	1.3 0.4 0.2	5 1.0	06 0.1	0.8	1.00	71:	12.8	2.6	0.7	0	0.8	1.2	3.3	2.1	1.5	خ .و	3.5	0.2 0.4
4	1.3 0.4 011	5 0.9	060	0.7	1.0 0	60.1	0.8	0.6	2,6	.0.1	aF	1,3	0,3	a. '	2.5	2.8	315	1.23.6
5	1.2 04 0.1 0	5 2.8	2.7 0.1	2.8	3.7 0	6 000	0.2	2.6	27	0	0.8	0.9	3.	7.	1.6	1.3	9.5	2.2 2.6
6	1.3 0.4 0.1 0	5 0.8	06 0	27	100	1. 2.2	13.5	م رو	2.7	2	2,7	1,2	0.3	2./	21.5	1.7	7.3	12/15
7	1.3 0.4 0.1 4	5 0,8	06 0.1	0.8	120	1 2%	0.9	2.7	67	0	0.8	1,2	r. n	7 ·	ج. در	1.3	2.4	1.1 36
8	1.3 0.4 0.1 2	5 0.9	0.7 0.1	0.7	2.9 2	6 11	108	0.6	2.8	6	0.8	101	0.3	2.	1.5	3.1	1.3	1,2 1,
9	1.4 0.5 0.1 4	5 0.9		0.7	0,20	.7 0.1	0.9	16	0.7	^	0.8	1.1	1, 5	2.1	1,5	7	24.	11/26
10	1.2 0.4 0.2	5 0.8	0,70	0.7	2.7 0	6 11	2.8	dif	7	1	19	4/	1,3	21	2.5	2.7	14.	1.2 2.3
		-																
Average	1.27 0.41 0.12	.50 0.86	2,64 -0,06	074	0.97 0	62 315	0.83	0.63	0.70	0,01	0.83	1.76	7.27	0.10	0,50	0.28	246 7	17 059

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Screen # 18	en Diameter (in) 16 Exposed (in) 5 Submerged (in <u>) 70</u>	Forebay Ele	evation <u>' = a.'</u> al Flow 1100 cfs	Date Pers	-/26/25 onnel <u>ital fr</u>
Time Start //42	1/42				
Time End //46 Unit 223 /020	924 818				
Location U (C) L	U (C) L	U C L	UCL	U C L	UCL
Depth 0.2	0.8	0.08a	0.9	.05	0.5
Vector S A -V A	S A -V A	S A V	S A V	SAV	SAV
	1.0 0.4 0.1 0.5				
2 1.2 0.2 0.1 0.4	1.0 0.4 0 0.5				
3 1.3 0.2 0.2 0.4	1.0 04 0-1 0.5		<u> </u>		∤ }
4 1.2 0.2 0.1 0.3	1.0 04 0 0.5		↓	 	{
5 1,1 0,3 0.1 0.4	1.0 0.4 0 0.5		√	 	┨┠┈┼┈╎┈╏┈ ┤
6 /1/ 0.20.10.4	1.0 0.4 0.1 0.6		┤ ├── ├ ──	{ 	{
	1.0 0.4 0.1 0.4		┨┠┈┨┈┤┈	┃ ┃	
8 1.1 0.2 0.1 0.4	29 2.4 0 0.4	│	┨ ┈┈┤┈┤ ╌┼┈┈	╎ ┝ ┈╎┈╎┈	{}
9 1.3 0.7 .2.1 0.4	1.0 0.4 0.1 0.5	<u> </u>		{} }}-	┨╏╼╼╏╼═ ┪
10 1.2 0.2 0.1 0.4	0.9 0.4 0 0.5		┛┞╌╌ ┞ ╌╌┦┈╌	l	l
Average 1./8 0.23 2.15 0.3 Minimum 1.1 0.2 -0.t 0.3 Maximum 1.3 0.3 -0.1 0.4	0,9 0.4 -0.1 0.4				

Screen #	l	9		Scre	E	xpos	ed (in) 'á in) 🛂	(7	_	oreba	ay Ele Cana	evation al Flow	<u>(3)</u>	=3.1 /100	e ts				Date_ Perso	onnel	12 6, Ca	/844 In / A	crs T
Time Start	_	111	7			/11	7																	
Time End		117	,			112	7									`								
Time End Unit	87	2 3	10	2.0	8	24	8	18																
Location	ι) (c) l	.	U	Œ	5		U		:	L,	U	C				С			U	c		
Depth		0.2				0.8				0.08a				0.9				.05				0.5		
Vector	S	Α	-٧	4	S	Α	4	A	S	Α	٧		S	Α	٧		S	Α	٧		S	Α	V	
1	1.2	0.3	0.1	0.4	1.1	0.3	0.1	0.4 0.5 0.4 0.5																
2	1,2	1.3	0.1	0.4	0.9	0.3	0.1	0.5																
3	1.2	0.3	0	0.4	1.0	0.3	0	04																
4	1.2	0.3	0,1	0.4	1.1	0.4	011	0.5																
5	1.2	0.3	0.1	0.4	1.0	0.4	0.1	0.6																
6	1,1	0.3	0.7	0.4	0.9	0,4	0.1	0.5																
7	/./_	0.3	3.2	0.4	0.9	04	0	0.5																
8 9	1.1	0.3	0.2	0.4	1.1	0,4	0.1	0.4																
9	1.2.	0.2	0.1	0.4	1.1	24	0.1	0.5																
10	1.2	0.3	0.1	0.5	1.1	0.4	0.1	0.5 0.5 6.5				П												
Ī																			•					
Average	1.17	0.29	-412	0.41	1.02	0.37	401	0.48																
Minimum	1.1	0.2	0.7	0.4	8.9	0.3	-0.1	0.4														$\neg \neg$	$\neg \uparrow$	\neg
Minimum Maximu	m /	12 C	30	0.5	1.1	0,4	0	0.6																

Screen #	20 Scree	en Diameler (in) Exposed (in) Submerged (in)	Forebay El	evation <u>630.1</u> al Flow- <u>1100 cfs</u>	Dale_ Perso	7/2 6 , 89 onnel <u>301/68.</u>
Time Start Time End Unit	///D ///4 823 /020	1110 1114 824 812				
Location	U C) L	U (C) L	U C L	U C L	U C L	U C L 0.5
Depth Vector	0.2 S A -V A	S A -V A	SAV	SAV	SAV	S A V
Vector	0.7 0.3 0.1 0.4					
2	1.1 0.2 0.1 0.4					
3	0.8 0.3 0.1 0.4					
4	0,9 0.2 03 0.4	1.0 0.5 0.1 0.5	1	╢┷┼┷┼┷		
5	1.1 8.3 0.2 0.4	0.9 01 0 0.5	1	┤ ├─ ┤ ─┤──	 	(}
6	1.2 0.3 0 3.4	09 0.4 0.1 0.4		_	 	┃ ┃──┃
7	1.0 0.2 0.2 0.4	0.9 0.4 0.1 0.4	11	┨┠──╂──╂──	┨ ┝═╌ ┼╌╌┼╌╌	┨ ┍┈┼┈╏┈ ┪
8	1.0 0.2 0.1 0.	10.9 0.4 0 0.5	{ 	┨ ┈╏┈╏┈╏┈	┃ ┣ ┈┃ ┈┃┈	│ │ │
9	1.1 03 0 04	0,8 0.3 0.1 0.5		┨┞┈═╏╼╌┠═╸	┨┠ ┈╌╏┈╶╏ ╌┈	│ ├├ ┤
10	1.0 0.3 0.1 0.4	1.0 04 0.1 0.5	1	<u> </u>	<u> </u>	
			<u> </u>	7		
Average	0.99 0.26 0.12 0.40	0 294 040 -007 048	┦┝ ┷┼┷┼┷	┨┠╼╂╾╂╾╏	 	
	n 0.7 0.2 -0.3 0.4			┨╏┈╏┈╏┈╏	┨┠╼┼═┼═┼═	
Maximun	n 1.2 23 0 04	1.1 0.5 0 0.5	J		# 	J

Notes: Erra tic Sweep/Appro ach at 0.2 2

Forebay Elevation 535./
Canal Flow 100 cfs Personnel 40 /FET Screen Diameter (in) 162 ,' Screen # 2/____ Exposed (in) 50 Submerged (in) スタ 1104 Time Start 1104 Time End 1107 1107 Unit 1020 824 818 U (C) Location U C С Depth 0.08a 0.9 .05 SAV Vector SAV s l A V AV 0.8 0.5 0 0.8 0.4 0.1 0.7 0.4 0.1 1.3 0.2 0.1 0.4 Average 1.25 0.18 -0.12 0.46 0.80 1.47 -0.06 0.52 Minimum 1.2 0 -0.2 0.4 0.7 0.4 0.7 0.4 Maximum 1.3 0.3 0.1 0.4 0.9 6.5

Notes: Exectle vendering of one (pordie)

Screen #	1056	en Diameter (in) // Exposed (in) 5 Submerged (in) /056	Cana 1/32	vation 6 30. 1 Flow 1/00 c fs 1/32 1/37	0134	7/24-21/84 onnel <u>%/Phy</u>
Time End Unit	7100	/100	1/37	-"3/		
Unit		 				
Location	UCL	UCL	UCL	UCL	υ©ι	L C L
Depth	0.2	0.8	0.08a	0.9	.05 S A -V A	5 A V A
Vector	S A -V A	SAVA	S A V	S A V D8 26 0 28	S A -V A	2.7 2.1/ 0.1 0.5
1	1.1 0.3 0 0.5	0.7 0.5 0 0.5	1.0 0.5 0.1 0.7	0.8 26 0 28	1.1 0.2 0.1 3.4	
2	0.9 0.5 0.2 0.5		1.0 0.6 0.1 0.7	2.2 2.6 -2.1 2.5	1.0 2.20. 0.4	1.5 2.5 0 0.4
3	1.0 0.3 0.1 0.5			0.7 03 0 09	1.2 0.2 0.1 0.4	0.8 0.4 0 0.5
4	1.1 0.3 0.1 0.5	0.6 0.5 0 0.6	2.3 0.5 0.1 2.7	0.6 0.0 -01 0.7	1.20,20,10.4	
5	1.1 0.5 0.1 0.5	06 06 0 0.6	2205 227	0.5 06 -0.1 0.7	1,20,30.104	
7	1.1 0.4 0.1 0.5	(06 25 01 27	1.2 0.3 0.1 3.4	1.0 0.4 0.1 22
8	1.0 0.4 0.1 0.5				1.2 0,2 0,1 3,4	2.7 2.3 3.1 2.5
9	1.1 0.3 0.1 0.5		1.00.50.12.7	13 013-01 08	1.2 20 3.1 9.4	2.4 1.3 2.1 2.5
10	1.1 0.3 0.1 0.5		1,0050 00	03 02 01 28	1.1 00 32 30	1.8 2.4 0 2.4
10		<u> </u>				
Average /	05 636 0 11 0.50	a65 0.48 -0,0 0.54	0.97 0.53 -0.07 0.67	0.58 0.600.08 0.74	1.15 0.24 0.10 0.4	0.90 0.36 -0.06 0.40
Minimum						
Maximum						
Notes: (, ,	+ 0) 7 60H	· of			

Erratic readings of 0.2 2 same of

Forebay Elevation 630.1 630.0 Date 7/26/89

Canal Flow 1/00 - 1 037c f5 Personnel Cta/A

, Screen # 24

Screen Diameter (in) 162 ·· Exposed (in) 54

Time Start	1046 7/26	1046 7/16	1/24 7/27	1124 7/27	0926 7/27	0926 7/27
Time End	1051	1051	1/29	1/29	09:50	2725
Unit	823 1020	824 818	823 /020	824 8/8	823 1020	824 818
1=111		<u></u>	<u> </u>			
Location	U (C) L	U C L	U C L	UCL	U C L	UCL
Depth	0.2	0.8	0.08a	0.9	.05	0.5
Vector	S A -V A	SAVA	s A -V A	S A V A	S A -V A	SA-VA
1	1,1 0.3 -0,1 0.5	0.9 0.4 0 0.5	1.2 06 0 0.7	1.1 06 -0.1 2.6	1.2, 0.3 0.1 0.5	1.0 03 0 0.4
2	09 04 01 05	1.0 0.4 0 0.5	1.1 0.5 0 0.7	1.0 0.6 -0.1 3.7	1.3 3.3 3.1 3.	1.1 2.4 0.1 2,5
3	0.8 0.3 0.1 0.5	0.9 05 0 0.5	1.2 0.6 0 0.7	0.9 26 -21 0.7	12 0,3 2. 25	1. 0.1 0.1 0.0
4	1.1 0.3 0.1 0.5	1.0 0.4 0.2 05	1.1 0.5 0 0.6	1.0 00 -0102	1.3 0.3 01/05	11/ 101 0 0.5
5	0.8 0.3 0.1 0.5	1.0 0.4 0.0 65	1.2 0.5 0 0.7		12 2.3 0.5 25	1.0 2.4 0.1 0.5
6	1.0 1.3 0.2 0.5	0.9 0.5 0 0,5	1.1 3.6 0.10.7	1.0 0.6.0.1 2.7		17 25 0 26
7	1.2 1.3 0.1 0.5	0.8 0.5 0 05	1.20,60,10.8	1.2 0,6 -0,10.8	3.5 3. 3.5	13 73 0 75
8	1.1 0.2 0.1 0.5	1.0 0.4 0 2.5	1.2 0.6 0 0.7	0.9 04 12 0.7	32 3.4 0.1 3.5	43 34 24 3.5
9	1.0 0.4 0.2 0.5	1.0 0.4 -0.2 0.5	1. 16 -6.1 0.7	1.0 0.6 0 0.7	1.1 0.0 0 25	1.0 100 100
10	0.6 0.3 0.1 0.4	0.4 0.4 0.2 0,5	1.1 36 0 2.7	1.0 3.6 -040.7	1 1,3 2 2.5	1.2 2.4 2 7.5
Average	237 231 -212 0.49	2.94 0.43 000 0.50	1.16 057 TO 11 070	1.01 040 0.10 0.69	1,21 0.31 -0.10 0.9	1.03 0.39 -0.05 0.51
Minimum						

Notes: 823:
$$x = +A$$

 $y = +S$
 $1050 x = -V$
 $y = +A$
 $y = +A$
 $y = +A$
 $y = +A$
 $y = +A$

Erratic readings perid really at 0.2 ? (turbulence?)

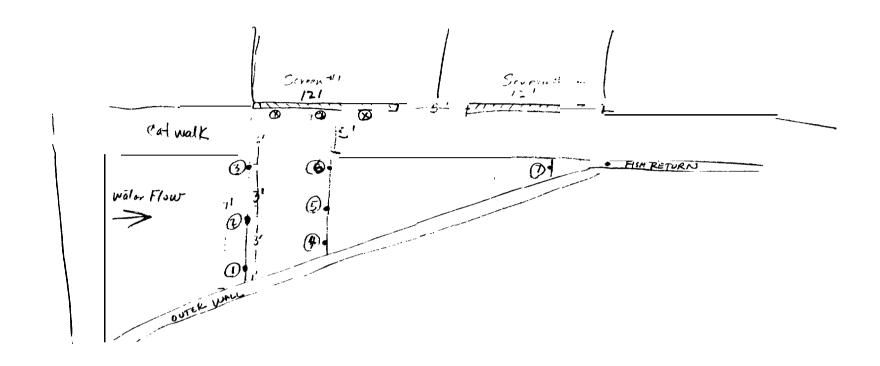
Screen #23 out of sorvice.

Screen Diameter (in) Exposed (in) Submerged (in)	Forebay Elevation 630/ Canal Flow 1/00 c A	Date 7/24/94 Personnel @ca/ FB 7
Time Start 1412 (412 Time End 1417 1417 Unit 923 1020 924 818		
Depth 0.2 0.8	U C L U C L 0.08a S A V S A V	U C L U C L .05 S A V S A V
Average /. /x Minimum Maximum Notes: 824 = †x +A + +y = s 217. +x = V y : †A		

+ A 15 Urstream

Bypass Sereen #	2		•	Scree	en Dia Ex Subn	amete (pose nerge(r (in) d (in) d (in)			F - -	oreba	a y Ele Cana	evation Il Flow		<u>63</u> 1100	e /s				Date_ Perso	onnel 🧃	: 5 ' !43 .	د م <u>م</u> ۱ <u>۲۵</u>	<u></u>
Time Start	1	42	5			142	5																	
Time End Unit	22	4 3 0		20	8	143 24		18																
Location	U	G) [C) ı		U	С	;]	L	U	С	, 1		U	С			<u>U</u>	С	L	
Depth	L	0.2			L	0.8				0.08a				0.9				.05		i	Ĺ	0.5		
Vector	S	Α	7	A	S		-٧	A	S	Α	V		S	Α	V		S	Α	V		S	Α	٧	
1	1.8	0	02	-91	1.4	-42	-0.3	0			<u> </u>				<u> </u>	<u> </u>	L		<u> </u>		Ш			
2	4.7		-a2		1.4	-0.3	72.3	-00/			<u></u>					Ш	L		<u> </u>	Ш				
3	1.8		-0.1		1.5	-0.2	-0.3	0	<u></u>			<u> </u>				Щ	L							
4	1.7		0.2				~0,3			L	<u> </u>	<u> </u>			<u> </u>	Ш								
5	1.8		-0.2		1.6	-0.2	2.3	-0.1	L											Ш				
6	1.7	0	0.7	0.1	1.3	-0.2	-0.4	-0.1		Ü.,														
7	1.7	0	70.7	0	1.5	-0.3	-0.3	0																
8	1.7			0.1			·0.3					П				П								
9	1.7		0,2		1.6	0,3	-0.3	-0.1															\neg	
10	1.7	-0.1	-0.2	0	1.6	-0.3	-0,3	-0./								\Box						\Box	$\neg \neg$	\neg
Average	1.73				1.49																		\Box	
Minimum											Γ												\neg	
Maximum	_																							\neg

BYPASS Sereen #	3	Scree	n Diameter Exposed Submerged	Exposed (in)													nnel _	3 / A	<u> </u>	<u>/^</u> -
Time Start Time End Unit	1437 1442 823		824																	
Location	U O	L	UC	L	U	С	L		U	С			U	<u> </u>			U	C	<u>L</u>	
Depth	U (9)		0.8		0	.08a				0.9	,		<u></u>	.05			ļ	0.5		—
Vector	SA		SA	-V A	S	Α	٧		S	Α	V		S	A	V	\square	S	Α	<u> </u>	
1	1.4 -0.1 -0	.2 -0.2	1.2 -0.3																— ↓	
2	1.4 -0.1-0		1.2 -0.3	0.5-0.6												Ш				
3	1.4 -0.1-0		1.3 -0.3	0.5 -0.5																
4		20	1.3-0.4	0.5 -0.4																
5	1. 2 -3.1-	12 -4.1	1.3-0.2	0.5 2.5																
6		7.20	1.2-0.3	-1-25																
7		,20.1	1.2 03	15-26																
	13 4	17 01	1 2 4 2	201-05																
8	1.3 D 0 1.4 0 0	7 201	1/3/5	-45 -23	-															
9	7,7 0 6	2 7 7 4	13 6 4	-44.4	-		-													
10	7.4 FO.7 -	7.0 7.1	(.) [7.7]	717 710	L	L	<u> </u>	لـــــا	Ь—	Ь	ــــــــــــــــــــــــــــــــــــــ	I			·					
							Γ				Τ	T		Г						\Box
	3/ 0.460.	74	1.36		-	-		\vdash	 	 	1			\vdash		\Box				
Minimum							├	 	-	├─	\vdash	1		 	 					
Maximum					<u> </u>	1	1	لـــــــــــــــــــــــــــــــــــــ	 _	Щ	<u> </u>		l	<u></u>	L	لــــــا	L	ا ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ ـ		



Sep CL S cross I U	pper Trensert	en Diamoner (in)	Forebay Flo	reg Facility Flow Measure 630.0 (Sovation 627.5 (Sovation Flow //3200)	rements (meus) Prohombes Date Perso	7/25/84 onnel <u>100 /84</u> 7
Time Start	1005	1005	1018	1018	1025	1025
Time End	1011	1011	1022.	/122_	1030	1030
Unit				<u> </u>	<u> </u>	<u> </u>
	1	1	Z	2	3	
Location	U C L	UCL	UCL	UCL	U C L	U C L
Depth	0.2	0.8	0.08a 0.2	0.9 0.8	-05-0,2	- 0.5 -0,8
Vector	S A -V A	S A -V A	SAVA	S A -V A	SA-VA	SAVA

Average 1/7 (37 1039 6.52	0 027 0.01 0.28 1.7	1.76-0.07-0.24 0.19 0.01 0.14-0.20 0.18 1.90-0.36-0.36-0.34 0.41 0.01 12.19-0.14 0.40
Minimum		
Maximum		

0.1

-43

-02 0.2

25

1.3 .0.1 0,1 0.2

1.8-04

1,8 1,8 0 1.9 -01 0.1

0

-03

0,3 0,3 0

0.3

-0.2

0,3 -0.1

-08 o.U

-08 04

0

Notes:

2

3

5

6

94" deep 0.2 = 19" from surfaces 0.8 = 75 " from surfaces

0.8 0.6 0.9 1.4 0.2 0.3 0.7 0.5 0.6 -0.1 0.5 0.5

0.4 0,4 0.5

0.8 0.6

-0.1 0.3 0 0

0,1

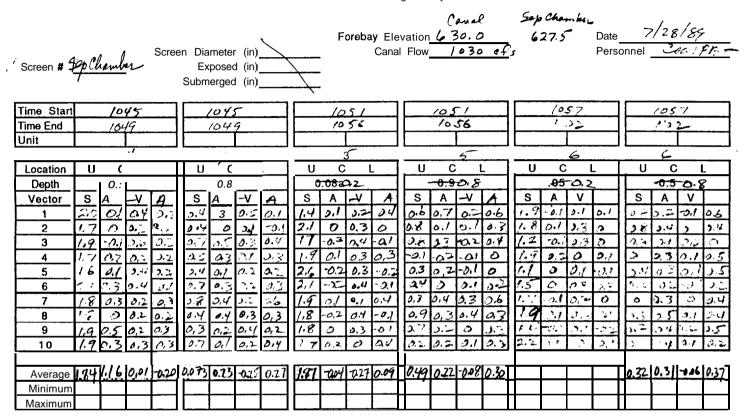
2,8

0.1

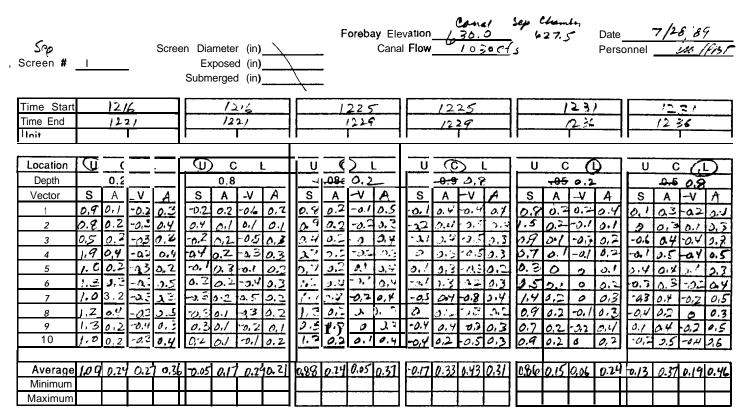
0

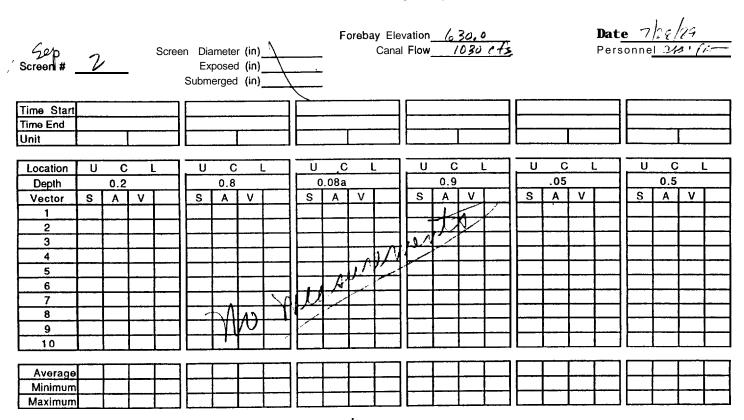
0.1 0.5 C.1 0,2 0 0.3 -0.1 0,1 0.3 0.4 0.2 0.1

1.2 0.1



Sep Ch	am bar	Scree	Ex	posed		_	$\overline{}$	Fo							efs	Sop. C 6:	hamb, 27,5	4	Date_ Perso	7/2	8/8°	1 4/po	<u></u>
			Guom			_				184	, _ ^	e											
Time Start	1108		<u></u>	110	<u>e </u>	_			<u> 21 </u>		L		112			-				-			
Time End						4			25		<u> </u>		//2	3_						\vdash			
Unit	<u> </u>		L			J					<u> </u>					L	اـا		لـــــا	L			
	7	·		7	<u> </u>				FR.		-		FR						— ₁	U	C		
Location	U C	ᆜ	U	С	<u> </u>	4	U	С			-	U	<u></u>			U		<u>.</u>	-	F-0	0.5		\vdash
Depth	0.2		<u></u>	0.8		4			~ ∪,		-			0.8			.05	٧		s		V	
Vector	S A -\		S		<u>-v / ^</u>	_	S	Α	_*_		5		Α_	~	A	S	Α.	- V	-	19	Α	_	
1	15 02 0	23:-	;. <u>)</u>	0.2		<u>"</u>	1.7		_	0,1	1.	-+		-3.3	3,1	-				-			
2		101	1.1	0.4	02 34	_	1.5	-0,2		-0.1	1,	_	<u> </u>	0.2									\dashv
3		3 0.4	1.0	0.3			1.9	0	0	0				-0.1	2	<u> </u>				\vdash			
4	1.6 0.3 01		0.9		210		1.6		0	01			<u> </u>	-01	3	 				-			
5	1.7 03 0	20,3		0,5			1.5		0	-01		_	a/	2	- 2.1					 			\dashv
6	11-0-20	2011		0,2					3.1	Q.	114		0.1	-0.1	-	\vdash				\vdash			-
7	18 CA 0	2 0.1		0.4			1.7	-0.1		0			0	0	0	-				 			
8	1,4 0.20		58	0.4	0.2 0,	<u>'/</u>	2,0		•	0	<u> 6</u>		<u>ə</u>	0,1		-				—			-
9	1.6 0,30.	2 0.2	1.0		23 2.	5		-0.1	0.1	0	<u> </u>	_	0	-0.1		 				—			-
10	1.6 0.21	3 0.3	30	0,3	0,0		1.8	0	0	0,1	1.	٤	0	-0.1	0.1	l L	L	L	<u> </u>	L			نـــا
											_												
Average	164 0.26 -0	21 0.29	099	0.35	-0.18 0.	46	1.15	10,08	70.04	0.01	1.3	25	-0.0	0.04	0.02		ļ			 		-	
Minimum						_					<u> </u>	_				 			 	ļ			
Maximum				1	l_	╝									.	L	L	L		L			





APPENDIX D

EASTON SCRFENS RAW DATA SHEETS

APPEMDIX Q

EASTON SCREENS RAW DATA SHEETS

This appendix contains the raw data sheets for flow measurements taken at the Easton Screens on June 14 and 15. 1989. Page D. 2 shows the calculations made to position probes at the proper depths and the raw data from measurements taken with a unidirectional flow meter. Raw data for measurements taken behind each of the drum screens with a bidirectional flow meter are found on pages D. 3 through D-11.

DATE: 6/14/84

Measurements Using Marsh Mc Birvey Model 201 Canal = 1130 cfs Csa WATER CURRENT METER

	0. 2	P. DEPTH	0. 8	DEPTH		
SCREEN	TIME	VELOCITY	TIME	VELOCITY	COMMENTS	Ave.
1	1258	0.15	1143	0.05		0.10
2	1360	0.15 (1140	0.15		0.15
3	1301	0,20	1138	0,20	-	0.20
4	1303	0.20	1136	0,20		0.20
5	1306	0.30	1/34	0,35		0.325
6	1307	0.30	1132	0.30		0.30
7	1414	0.35	1417	0.45		0.40
8	1412	0.35	1419	0.50		0.425
9	1408	0.45	1422	0.50		0475
10	1343	0.35 .	1423	0,50		0.42
11	1341	0.35	1420	0.50	-	0.424
12	1540	0,40 *	1426	0.60		0.50
13	1309	0.40	1130	0.50		0.45
14	13/0	0.40	//28	0.55		0.419
15	/3/1	0.45	1126	0.55		0.50
16	13/4	0.40 * 1	1124	0.55	Varied from 0.3-0.6	0.475
17	1315	0,55	//22	0.70		0.645
18	1317	0.45	1119	0.65		0.55

NOTES

139" TOTAL Depth Measurements taken . fi downstream side of severe at screen centurline sensor positioned a even with stoplog slots, . rabout 12"-18" dowstream of the scoren diameter,

0.82=111.2.

0.22: 17.8"

Conduit -Chap

The or measurements were . MARLER Using. Marsh- Mc Bildy Model 201 water Current Motor

Nersurement on Screens 1-6 and 13-18 were wade when screens 7-12 were not farming. (BR changing of 1/8 n mg tors). All screens were revy clean, how over.

Screen Bay X-section 147 44 wide

DATE: 6//5/84
TIME START: 271/
TIME STOP: 0904

SCREEN

✓

Measurements with Marsh McBirney Mo de / 511 Water Current Meter

Bypass Flow = 40 cfs (20 ca.) CAR

	0. Z	DEPTH
SCIEEN	SWEEP	APPROACH
Ž	-0.8	D.
2		
4	0.1_	0
5	0.1	0
6	0.1	0
7 0.14	0.1	-0.1
8 0-14	0.1	-0.1
9	0.2	0
10	0.2	0

AVERAGE	£ 0.06	-0.02
MIN -	0. 1	-0.1
MAX	0.2	ó

	DEPTH	
SWEEP	APPROACH	COMMENTS
-21	0	
-0.I	0	
0	0	
0.1	0	
0.1	0	
0.1	0	
0.1	0	
0.1	0	•
0.2	0	
0.1	0	

0.06	0	
-0.1	0	
0,2	0	

DATE: 6//5/89
TIME START: 09 TIME STOP: 09

SCREEN # 2

O. 2 DEPTH

SWEEP	APPROACH
0.1	0
0.1	0
0.2	0
0.2	0
	0
	0
	0
	0
	0
1.0	0
֡֡֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜	0.1 0.2 0.2 0.2 0.2 0.2 0.0

AVERAGE	0,11	0
MIN	0.0	0
MAY	0.7	A

	DEPTH	
SWEEP	APPROACH	
0.2	0	
0.2	O	
0.2	0	

0

0.2	0		
0.1	0		1
0./	0		
0,1	0	1	
0.1	[2		
0.17	0		
0.1	0		
0.3	0		

COMMENTS

Note: "Sweep" is velocity perpondicular to screens
"Approach" is velocity parallel to screens. + Reading is downstream, or
normal flow direction.

Sweep velocity (+)

"Approach" velocity (+)

DATE: 6//5/89
TIME START: 09/6
TIME STOP: 09/9

SCREEN #3

O 9 OEDTH

_	U. &	ULPIN
SCREEN I	SWEEP	APPROACH
1	0.2	0
_ 2	0,2	0
3	0.1	0
4 0.22	0.2	-0.1
5	0.2	0
6	0,1	0
77	0.1	0
8	0.1	0
9	0.2	0
10 0.14	0.1	0.1

0.8	DEPTH	
	APPROACH	COMMENTS
0.2	0	
, O, Z	0	
0.2	0	
0.2	0	
0.2	0	
0.2	0	
0.2	0	
0.2	0	

AVERAGE 4	0.15	0
MIN	0.1	-0.1
MAX	0.2	0.1

15.0	0	
0.2	0	
0,3	0	

DATE: 6//5/69
TIME START: 0913
TIME STOP: 0926

SCREEN خ 🗸

O. 8 DEPTH
SWEEP APPROACH

		DEPTH
SCREEN	SWEEP	APPROACH
1 ,/4	0.1	0.1
2 ,36	0.3	-0.2
3	0.2	0
4 114	0,1	0.1
5 .32	0.3	-0.1
6	0.3	0
7 .22	0.2	0.1
8 .20	0.1	0.2
9	3	0.2
10 -23	0,1	0.2

0.2	0	
10.2	c	
0.3	G	
0.2	0	
0.3	C	
0.3	-0.1	0. 37
2.3	0	
0,3	0.1	0,32
0,2	0	-
0.2	0.1	0,22

COMMENTS

-		
AVERAGE)	C.17	0.06
MIN	0.0	-0.2
MAX	0.3	0.2

DATE: 6/15/89
TIME START: 0929
TIME STOP: 0932

SCREEN #5

	0. 2	DEPTH
SCREEN	SWEEP	APPROACH
1	0.2	U
2	0.3	0
3	0.2	0
4	0.2	0.1
5	0.2	0.1
6	0.2	0
7	0.2	0
8	0.3	0
9 72	0.2	0.1
10	0.3	0

AVERAGE,24	0.Z3	0.03
MIN	0.2	0.0
MAX	0.3	0.1

	DEPTH	
SWEEP	APPROACH	COMMENTS
0.2	0	
0.3	0	
0.3	0	
0.3	0	
0.3	0	
0.3	0	
0.3	0	
0.	0	
0.4	0	
.410.4	-0.1	
310.31	-0.01	
0.2	-0.1	
0.4	0.6	

DATE: 6//5/89
TIME START: 0934
TIME STOP: 0939

SCREEN #6

	0. 2	<u>DEPTH</u>
SCREEN	SWEEP	APPROACH
1	1 0.2	-
2	0,4	0
3 .41	0.4	-0.1
4	0.3	0
5	0.3	0
6	0.2	0
7	0.2	0
8	0.2	0
9 .22	0.2	-0.1
10	0.2	0

AVERAGE 26	0.26	-0.02
MIN	0.2	-0.1
MAX	0.4	0.0

٠. .

0. 8 DEPTH

SWEEP	APPROACH	COMMENTS
0.4	I 0	1
0.4	0	-
\$20.3	-0.1	
6.4	0	
32 0.3	0	
32 0.3	01	
0.2	0	
0.3	0	
	0	
0.3	0	
功 0.33	0	·
33 0.33 0.2 0.4	-01	
0.4	0,1	·

DATE: 6/15/89
TIME START: 6942
TIME STOP: 6945

SCREEN #フ

0. 2 DEPTH

	U. ~	
SCREEN	SWEEP	APPROACH
1 .2.2	0.3	0.1
2 .22	0.2	0.1
3 ,22	0.2	0.1
4 -22	0.2	-0.1
5 👉	0. 3	-0.2
6 . 2 2	0.3	0
7,20	0.2	0
8 ,22	0.2	0.1
9 .50	0.2	0
10 62	0.2	0.1
10 조각	0.2	0./

AVERAGE0.29	0.23	0.02
MIN	0.2	-0.2
MAX	0,3	0.1

Λ	R	DEPTH

SWEEP	APPROACH	COMMENTS
0.4	0	
0.4	0	
32 0.3	0.1	
0.4		
0.3	0	
320.3	0,1	
0.3	0	
320.3	0.1	
0.3	0	
0.3	0	
34 0.33	0.03	
0.3	0	
0.4	0.1	

DATE: 6/15/65
TIME START: 0948
TIME STOP: 095/

SCREEN

0.2 DEPTH

U. &		
SCREEN	SWEEP	APPROACH
1	I 0.3	0
2 ,4	5 0.4	-0.2
3	0.2	0
4	0.4	0
5 ,41	0.4	-0.1
6	0.4	0
7	0.3	0
8 ,41	0.4	-0.1
9 , 11	0.4	-0.1
10	0.4	-0.2

AVERAGEISA	0,36	-0.07
MIN	0-2	-0.2
MAX	0.4	1.0

0.8 DEPTH

SWEEP	APPROACH	COMMENTS
11 0.4	-0.1	
6.4	0	
0.4	0	
0.4	0	
0.4	0	
510.5	-0.1	
0.5	0	
0.5	0	
141 0.4	-0./	
0.4	0	
10		

o. ··		
0,43	-0,03	
0.4	-0.1	
0.5	0.0	

0.8 DEPTH
SWEEP APPROACH

DATE: 6/15/89
TIME START: 0957
TIME STOP: 0957

SCREEN #9

0. 2 DEPTH

		DELLII
SCREEN	SWEEP	APPROACH
1	0.3	0
2	0.4	0
3	0.3	0
4	0	-0.1
5	151 0.6	-0.1
6	0.2	0
7	0.2	0
8	0.3	0_
9	0.3	0
10	0.2	0

- 1	0.4	<i></i>	1
.5	20.3	-0.1	Ι
	0.4	0	Ι
	0.4	0	I
	0.4	0	Ι
	0.4	0	Ι
0.1	17	•	
Г	0.37	-0.01	Τ

AVERAGE 0.	20.28	-0.02
MIN	0.0	-0.1
MAX	0.6	0.0

0.37		
0.37	-0.01	
0.3		
0.4	Ø. O	

COMMENTS

DATE: 6/15/64
TIME START: 1002
TIME STOP: 1005

SCREEN €/0

0. 2 DEPTH

0.			
SCREEN	SWEEP	APPROACH	
1 ,4	ال بك. يوم ان	-0.1	
2 132	0.3	-0./	
3	0.5		
4	0.5	0	
5 , 51	1 0.5	-0,2	
6 .7/	0.7	-0.1	
7 .6/	0.6	-0.1	
8 , 4	0.4	-0,2	
9	0.5	0	
10	0.4	6	

U.	ð	Ш	ľ	ď	1	H
			•	-	-	_

	APPROACH	COMMENTS
-		COMPLAIN
0.3	0	
0.4	0	
0.7	0	
610.6	0.1	
0.5	0	
0.5	0	
0.7	0	
0.5	0	
71 0.7	0.1	-
0.5	0	

AVERAGE 44	0.48	-0.08
MIN	0.3	-0,2
MAX	0.7	8.0 .

ๆป	0,54	0.02	
_	0.3	0	
1	0.7	0.1	

DATE: 6/15/84
TIME START: 1009
TIME STOP: 1012

SCREEN #//

0.2 DEPTH

	U. &	VEFIN
SCREEN	SWEEP	APPROACH
1 .22	0.2	-0.1
2	0.	0
3 .41	0.4	-0.1
4	0.4	0
5	0.4	0
6 .32	0.3	-0.1
7	0.3	6
8	0.2	0.1
9	0.2	0
10	0.4	0
-		

AVERAGE033	0.32	-0.02
MIN	0.2	-0.1
MAX	0.4	0.1

0.8 OEPTH

	APPROACH	COMMENTS
0.5	0	
.51 0.5	0.1	
0.5	0	
0.5	0	
0.5	0	
0.4	0	
0.5	0	
0.5	0	-
.5! 0.5	-0,1	
0.5	0	
	•	
0.49	0	
0.4	-0.1	
0.5	0.1	

DATE: 6/(5/8 9
TIME START: /0/5
TIME STOP: /6/8

SCREEN 4/2

O. 2 DEPTH

	0. 2	DEPTH		
SCREEN	SWEEP	APPROACH		
1	0.3	0		
2	410.4	-0.1		
3	0.3	0		
4	141 0.4	-0.1		
5	0.3	0		
6	141 D.4	-0.1		
7	32 0,3	-0.1		
8	0.4	0		
9	11 0.4	-0-1		
10	0.3	0		
AVERAGE	& 0.35	-0.05		
MIN	0.3	-0,1		
MAX	0.4	0.0		

0.8 DEPTH

SWEEP	APPROACH	COMMENTS
0.6	0	
0.5	0	
0.5	0	
0.5	0	
0.5	0	
0.4	0	
0.5	0	
0.5	0	
0.5	0	
0.5	0	
050	0	_
Ø. U	0	
•	0	

DATE: 6/15/54
TIME START: /0 2 2
TIME STOP: /0 2 5

screen ≠/3

SWEEP	APPROACH
41 0.4	-0.1
0.4	0
0.4	0
0.5	0
41 0.4	-0.1
0.4	0
0.2	0
0.3	0
11 0.4	-0.1
41 0.4	-0.1
0 . 38	-0.04
0.2	-0.1
0.5	0.0
	0.4 0.4 0.5 91 0.4 0.2 0.2 0.3 4 0.4 1 0.4

0.8	DEPTH

APPROACH	COMMENTS
0	
0	
0	
0	
0	
0	
0	
0,1	
0	
0	
	APPROACH O O O O O O O O

0.49	0.01	
0.4	o,	
.5	0,1	

DATE: 6/5/89
TIME START: /028
TIME STOP: /63/

SCREEN#14

	0. Z	DEPTH
SCREEN	SWEEP	APPROACH
1	0.3	0
2	41 0.6	-0.1
3	57 0.5	-0.1
4	410.4	-0.1
5	51 0.5	-0.1
6	0.4	0
7	0.5	0
8	0.4	0
9	.32 0, 3	0.1
10	0.6	0
0		

0,		
AVERAGE	0.45	-003
MIN	0.3	-0.1
MAX	6. 6	0.1

0.8 DEPTH

SWEEP	APPROACH	COMMENTS
0.5	0	
2.5	0	
0.5	0	
0.5	0	
0.6	0	
0.5	0	
0.6	0	
0.5	0	
5.6	0	
0.5	0	
		·
0.52	0	
1	0	
0,6	0	

DATE: 6//3/84 TIME START: /034 TIME STOP: /037

SCREEN /5

0.2 DEPTH

	₩. ~	DEI III
SCREEN	SWEEP	APPROACH
1 ,5"	b/s-	- 0. /
2 .<:	0.5	-0./
3	0.3	-0.1
4 ・ンン	0.2	-0.1
5 .6	0.6	-0./
6 .54	0.2	-0./
7	0.5	0
8 🐠	0.5	-0./
9	0.5	0
10 .01	0.	-0./'
,05	•	

	DEPTH	
SWEEP	APPROACH	COMMENTS
.510-5	0.1	
.320.3	-0.1	
0.6	0	
0.4	0	
73 0.7	0.2	
\$20.3	-0.1	
0.4	0	
,510.5	-0./	
0.6	0	
.510.5	-0.1	
B 11.65		

AVERAGE 0.44 -0.8 MIN 0,2 MAX

0,49		
0.48	-0.00	
0,3	-0.1	
OF	0,2	

DATE: 6/15/84
TIME START: 1044
TIME STOP: 1043

SCREEN #/6

A 9 DEDTH

_		DEPTH
SCREEN I	SWEEP	APPROACH
1	0.6	0.
2	0.5	0
3	0.4	0
4	0.6	0
5	0.4	0
6	0.6	0
7	0.5	0
8	0.8	0
9	0.4	0
10	0.4	0

SWEEP	APPROACH	COMMENTS
0.6	or /	
0.6	0	
0.6	0	
0,7	0	
1 0.6	0.	
0.	0	
0.7	0	
77 .	0.1	
0.6	0	
0.5	0.1	

AVERAGE 0.52 0 MIN 0 MAX

DATE: 6/15/39
TIME START: 1046
TIME STOP: 1049

SCREEN ¥/7

		0. 2	DEPTH
SCREEN		SWEEP	APPROACH
1		0.6	0
2	12	2 0.1	0.2
3		20.3	0.1
4	, 8	11 0.4	-0.1
5	•	11 0.7	-0.1
6	•	11 0.4	-0.1
7		11 0.4	0.1
8	,	13 0.7	-0.2
9	. 1	11 0.4	-0.1
10		0.5	0
		47	

		0	١.	8	_[) {	P	T	H	
-	7	-	=	_	_	٠.	_	_	-	

SWEEP	APPROACH	COMMENTS
0.4	0	
0.6	0	
.610.6	a/.	
0.6	0	
0.6	0	
0.6	0	
0.6	0	
0.6	0	
0.6	0	
0.6	0	

0.	4 +	
AVERAGE	0.45	-0.02
MIN	0.1	-0.2
MAX	0.7	0.2

0.58	0.01	
0,4_	0.0	
0.6	0.1	

DATE: 6/15/89
TIME START: 1052
TIME STOP: 1055

0. 2	DEPTH
	7

	U. & 1	
SCREEN	"SWEEP (APP ROACH
7	51 0.5	-0./
2	51 0.5	-0.1
3	0.54	
4	61 0.6	-0.1
5	4.0 11	-0.1
6	154 0.5	-0.2
7	51 0.5	-0.1
8	0.5	0
9	151 0.5	-0.1
10	51 0.5	-0.1
	9.51	

	9.51	
AVERAGE	0,50	-0,09
MIN	0,4	-1.2
MAX	0.6	0,0

0.8 DEPTH

	(APPROACH	COMMENTS
0.5	0	
0.6		
0.6	0	
0.6	0	
0.5	0	
5	0	
0.5	0	
0.6	-0.1	
0.6	0	
1	.0.1	
0.56	0.02	
0,56	-0.1	
0,	0.0	